## The dynamics of the quasielastic $^{16}{\rm O}(e,e'p)$ reaction at $Q^2=0.8~({\rm GeV}/c)^2$

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The physics program in Hall A at Jefferson Laboratory commenced in the summer of 1997 with a detailed investigation of the  $^{16}\text{O}(e,e'p)$  reaction in quasielastic, constant  $(\vec{q},\omega)$  kinematics at  $Q^2 \approx$  $0.8~({\rm GeV}/c)^2,~|\vec{q}|\approx 1~{\rm GeV}/c,$  and  $\omega\approx 445~{\rm MeV}.$  Use of a self-calibrating, self-normalizing, thin-film water target enabled a systematically rigorous measurement. Five-fold differential cross sections for the removal of protons from the 1p-shell have been obtained for  $0 < |P_{\text{miss}}| < 350 \text{ MeV}/c$ . Six-fold differential cross sections for  $0 < E_{\rm miss} < 120$  MeV were obtained for  $0 < |P_{\rm miss}| < 340$  MeV/c. These results have been used to extract the  $A_{LT}$  asymmetry and the  $R_L$ ,  $R_T$ ,  $R_{LT}$ , and  $R_{L+TT}$  response functions over a large range of  $E_{\rm miss}$  and  $P_{\rm miss}$ . Detailed comparisons of the 1p-shell data with Relativistic Distorted Wave Impulse Approximation (RDWIA), Relativistic Optical Model Eikonal Approximation (ROMEA), and Relativistic Multiple Scattering Glauber Approximation (RMSGA) calculations indicate that two-body currents stemming from Meson-Exchange Currents (MEC) and Isobar Configurations (IC) are not needed to explain the data at this  $Q^2$ . Further, dynamical relativistic effects are strongly indicated by the observed structure in  $A_{LT}$  at  $|P_{\text{miss}}| \approx 300 \text{ MeV}/c$ . For 25 MeV  $< E_{\rm miss} < 50$  MeV and  $|P_{\rm miss}| \approx 50$  MeV/c, proton knockout from the  $1s_{1/2}$ -state dominates, and ROMEA calculations do an excellent job of explaining the data. However, as  $P_{\rm miss}$ increases, the single-particle behavior of the reaction is increasingly hidden by more complicated processes, and for  $280 < |P_{\text{miss}}| < 340 \text{ MeV/}c$ , romea calculations together with two-body currents stemming from MEC and IC account for the shape and transverse nature of the data, but only about half the magnitude of the measured cross section. For 50 MeV  $< E_{\rm miss} <$  120 MeV and 145  $<|P_{\rm miss}|<340~{\rm MeV}/c,$  (e,e'pX) calculations which include the contributions of central and tensor correlations (two-nucleon correlations) together with MEC and IC (two-nucleon currents) account for only about half of the measured cross section.

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#### I. INTRODUCTION

Exclusive and semi-exclusive (e,e'p) in quasielastic (QE) kinematics [123] has long been used as a precision tool for the study of nuclear electromagnetic response [1–3]. Cross-section data have provided information used to study the single-nucleon aspects of nuclear structure and the wave functions of protons bound inside the nucleus, as well as to search for non-nucleonic degrees-of-freedom and to stringently test nuclear theories. Response-function separations [124] have been used to extract detailed information about the different reaction mechanisms contributing to the cross sections, since they are selectively sensitive to different aspects of the nuclear current.

Some of the first (e, e'p) energy- and momentumdistribution measurements were made by Amaldi *et al.* [4]. These results, and those which followed [1, 2, 5], were interpreted within the framework of single-particle knockout from nuclear valence states, even though the measured cross sections were as much as 40% lower than predicted by the models of the time. The first relativis-

tic calculations for (e, e'p) bound-state proton knockout were performed by Picklesimer and Van Orden [6-8]. Such Relativistic Distorted-Wave Impulse Approximation (RDWIA) calculations are generally expected to be more accurate at higher  $Q^2$ , since QE (e, e'p) is expected to be dominated by single-particle interactions in this regime of four-momentum transfer. Other aspects of the structure as well as the of reaction mechanism have generally been studied at higher  $E_{\text{miss}}$ . While it is experimentally convenient to perform measurements spanning the two excitation regions simultaneously, there is as of yet no rigorous, coherent theoretical picture that uniformly explains the data for all missing energy and all missing momentum. In the past, the theoretical tools used to describe the two energy regimes have been somewhat different. Within our present understanding, the regions are related mainly by the transfer of strength from the valence states to higher  $E_{\text{miss}}$  [9].

The nucleus  $^{16}$ O has long been a favorite for theorists, since it has a doubly closed-shell whose structure is thus easier to model than other nuclei. It is also a convenient target for experimentalists. While the knockout of 1p-shell protons from  $^{16}$ O has been studied extensively in the past at lower  $Q^2$ , few data were available at for any  $Q^2$  at higher  $E_{\rm miss}$  in 1989, when this experiment was first conceived.

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## A. 1p-shell knockout

The knockout of 1p-shell protons in  $^{16}\text{O}(e,e'p)$  was studied by Bernheim et al. [10] and Chinitz et al. [11] at Saclay, Spaltro et al. [12] and Leuschner et al. [13] at NIKHEF-K, and Blomqvist et al. [14] at Mainz at  $Q^2 < 0.4 \; (\text{GeV}/c)^2$ . In these experiments, the cross sections for the lowest-lying fragments of each shell were measured as a function of  $P_{\text{miss}}$ , and normalization factors (relating how much lower the measured cross sections were than predicted) were extracted. These published normalization factors ranged between 0.5 and 0.7, but Kelly [2, 3] has demonstrated that the Mainz data suggest a significantly smaller normalization factor (see also Table VIII).

Several groups [15–21] have recognized and calculated in detail the sensitivity [125] of the longitudinal-transverse interference response function  $R_{LT}$  and the left-right asymmetry  $A_{LT}$  [126] to spinor distortion, especially for the removal of bound-state protons. Such calculations predict that proper inclusion of these dynamical relativistic effects is needed to simultaneously reproduce the cross sections,  $A_{LT}$ , and  $R_{LT}$ .

Figure 1 shows  $R_{LT}$  as a function of  $P_{\rm miss}$  for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  for the QE data obtained by Chinitz et al. at  $Q^2=0.3~({\rm GeV/c})^2~({\rm solid~circles})$  and Spaltro et al. at  $Q^2=0.2~({\rm GeV/c})^2~({\rm open~circles})$  together with modern RDWIA calculations (see Sections IV and V for a complete discussion of the calculations). The solid lines correspond to the  $0.2~({\rm GeV/c})^2$  data, while the dashed lines correspond to the  $Q^2=0.3~({\rm GeV/c})^2$  data. Overall, agreement is good, and as predicted, improves with increasing  $Q^2$ .

## B. Higher missing energies

Not many data are available for  ${}^{16}O(e, e'p)$  at higher  $E_{\rm miss}$ , and much of what we know about this excitation region is from studies of other nuclei, mainly from <sup>12</sup>C. At MIT-Bates [22–26], in a series of  $^{12}C(e, e'p)$  experiments performed at missing energies above the two-nucleon emission threshold, cross sections much larger than those predicted by single-particle knockout models were measured [127]. In particular, Ulmer et al. [23] identified a marked increase in the transverse-longitudinal difference  $S_T - S_L$  [128]. A similar increase has subsequently been observed by Lanen et al. [27] for <sup>6</sup>Li, by van der Steenhoven et al. [28] for  $^{12}$ C, and most recently by Dutta et al. for  $^{12}\mathrm{C}$  [29],  $^{56}\mathrm{Fe}$ , and  $^{197}\mathrm{Au}$  [30]. The transverse increase exists over a large range of four-momentum transfers, though the excess at lower  $P_{\text{miss}}$  seems to decrease with increasing  $Q^2$ . Theoretical attempts by Takaki [31], Ryckebusch et al. [32], and Gil et al. [33] to explain the data at high  $E_{\text{miss}}$  using two-body knockout models coupled to final-state interactions (FSI) do not succeed. Even for QE kinematics, this transverse increase which starts at the two-nucleon knockout threshold seems to be a strong signature of multinucleon currents.

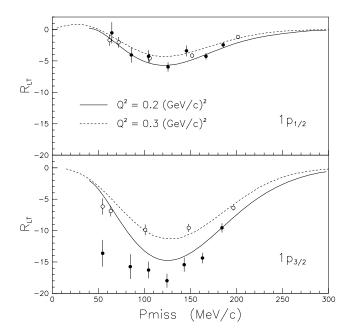


FIG. 1: Longitudinal-transverse interference responses  $R_{LT}$  as a function of  $P_{\rm miss}$  for the removal of protons from the 1p-shell of <sup>16</sup>O. The open and filled circles were extracted from QE data obtained by Chinitz et~al. at  $Q^2=0.3~({\rm GeV}/c)^2$  and Spaltro et~al. at  $Q^2=0.2~({\rm GeV}/c)^2$ , respectively. The solid  $(Q^2=0.2~({\rm GeV}/c)^2)$  and dashed  $(Q^2=0.3~({\rm GeV}/c)^2)$  curves are modern RDWIA calculations (see Sections IV and V for a complete discussion). Overall, agreement is good, and improves with increasing  $Q^2$ .

## II. EXPERIMENT

This experiment, first proposed [34, 35] by Bertozzi et al. in 1989, was the inaugural physics investigation performed in Hall A [36] (the High Resolution Hall) at the Thomas Jefferson National Accelerator Facility (JLab) [37]. An overview of the experiment apparatus in the Hall at the time of this measurement is shown in Figure 2. For a thorough discussion of the experimental infrastructure and its capabilities, the interested reader is directed to the work of Alcorn et al. [38]. For the sake of completeness, a subset of the aforementioned information is presented here.

## A. Electron beam

Unpolarized 70  $\mu$ A continuous electron beams with energies of 0.843, 1.643, and 2.442 GeV (corresponding to different virtual photon polarizations) and a typical  $\pm 4\sigma$  energy spread of 0.01% were used for this experiment (see Table I). Subsequent analysis of the data demonstrated that the actual beam energies were within 0.3% of the nominal values [39].

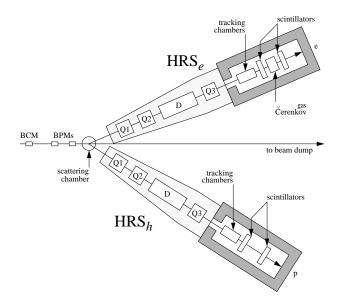


FIG. 2: The experimental infrastructure in Hall A at Jefferson Lab at the time of this experiment. The electron beam passed through a beam current monitor (BCM) and beam position monitors (BPMs) before striking a waterfall target located in the scattering chamber. Scattered electrons were detected in the  $HRS_e$ , while knocked-out protons were detected in the  $HRS_h$ . Non-interacting electrons were dumped. The spectrometers were free to rotate about the central pivot.

TABLE I: QE experiment kinematics were established within a constant center-of-mass energy framework. At each beam energy,  $|\vec{q}| \approx 1 \text{ GeV}/c$ . The angles  $\theta_{pq} = 0, \pm 2.5, \pm 8, \pm 16$ , and  $\pm 20^{\circ}$  correspond to central missing momenta of 53, 60, 148, 280, and 345 MeV/c, respectively.

| $E_{\text{beam}}$ (GeV) | $	heta_e \ (^\circ)$ | virtual photon<br>polarization | $	heta_{pq}$ (°)                |
|-------------------------|----------------------|--------------------------------|---------------------------------|
| 0.843                   | 100.76               | 0.21                           | 0, 8, 16                        |
| 1.643                   | 37.17                | 0.78                           | $0, \pm 8$                      |
| 2.442                   | 23.36                | 0.90                           | $0,\pm 2.5,\pm 8,\pm 16,\pm 20$ |

The typical laboratory  $\pm 4\sigma$  beam envelope at the target was 0.5 mm (horizontal) by 0.1 mm (vertical). Beam current monitors [40] (calibrated using an Unser monitor [41–43]) were used to determine the total charge delivered to the target to an accuracy of 2% [44]. Beam position monitors (BPMs) [45, 46] were used to ensure the location of the beam at the target was no more than 0.2 mm from the beamline axis, and that the instantaneous angle between the beam and the beamline axis was no larger than 0.15 mrad. The readout from the BCM and BPMs was continuously passed into the data stream [47]. Non-interacting electrons were dumped in a well-shielded, high-power beam dump [48] located roughly 30 m from the target.

## B. Target

A waterfall target [49] positioned inside a scattering chamber located at the center of the Hall provided the H<sub>2</sub>O used for this study of <sup>16</sup>O. The target canister was a rectangular box 20 cm long  $\times$  15 cm wide  $\times$  10 cm high containing air at atmospheric pressure. The beam entrance (exit) windows to this canister were 50  $\mu$ m (75)  $\mu$ m) gold-plated beryllium foils. Inside the canister, three thin, parallel water films served as targets. This threefilm configuration was superior to a single film 3× thicker because it reduced the target-associated multiple scattering and energy loss for particles originating in the first two films and it allowed for the determination of which film the scattering vertex was located in, thereby facilitating a better overall correction for energy loss. The films were defined by  $2 \text{ mm} \times 2 \text{ mm}$  stainless-steel posts. Each film was separated by 25 mm along the direction of the beam, and was rotated beam right such that the normal to the film surface made an angle of 30° with respect to the beam direction. This geometry ensured that particles originating from any given film would not intersect any other film on their way into the spectrometers.

The thickness of the films could be changed by varying the speed of the water flow through the target circuit via a pump. The average film thicknesses were fixed at  $(130 \pm 2.5\%)$  mg/cm<sup>2</sup> along the direction of the beam throughout the experiment, which provided a good tradeoff between resolution and target thickness. The thickness of the central water film was determined by comparing  ${}^{16}O(e,e')$  cross sections measured at  $|\vec{q}| = 330$ MeV/c obtained from both the film and a (155 ± 1.5%) mg/cm<sup>2</sup> BeO target foil placed in a solid target ladder mounted beneath the target canister. The thicknesses of the side films were determined by comparing the concurrently measured  ${}^{1}\text{H}(e,e)$  cross sections obtained from these side films to that obtained from the central film. Instantaneous variations in the target-film thicknesses were monitored throughout the entire experiment by continuously measuring the  ${}^{1}\mathrm{H}(e,e)$  cross sections. The scattered electrons and knocked-out protons passed through the 25  $\mu$ m thick stainless-steel canister side windows on their way into the spectrometers, depositing roughly 200 keV.

## C. Spectrometers and detectors

The base apparatus used in the experiment was a pair of optically identical 4 GeV/c superconducting High Resolution Spectrometers (HRS) [50]. These spectrometers have a nominal 9% momentum bite and a FWHM momentum resolution  $\Delta p/p$  of roughly  $10^{-4}$ . The nominal laboratory angular acceptance is  $\pm 25$  mrad (horizontal) by  $\pm 50$  mrad (vertical). Scattered electrons were detected in the Electron Spectrometer (HRS<sub>e</sub>), and knocked-out protons were detected in the Hadron Spectrometer (HRS<sub>h</sub>) (see Figure 2). Before the experiment,

TABLE II: Some results from the optics commissioning measurements.

|                    | resolution           | reconstruction           |
|--------------------|----------------------|--------------------------|
| parameter          | (FWHM)               | accuracy                 |
| out-of-plane angle | 6.00  mrad           | $\pm 0.60~\mathrm{mrad}$ |
| in-plane angle     | 2.30  mrad           | $\pm 0.23~\mathrm{mrad}$ |
| $y_{ m target}$    | 2.00  mm             | $\pm 0.20~\mathrm{mm}$   |
| $\Delta p/p$       | $2.5 \times 10^{-4}$ | -                        |

the absolute momentum calibration of the spectrometers was determined to  $\Delta p/p = 1.5 \times 10^{-3}$  [39]. Before and during the experiment, both the optical properties and acceptances of the spectrometers were studied [51]. Some optical parameters are presented in Table II.

During the experiment, the locations of the spectrometers were surveyed to an accuracy of 0.3 mrad at every angular location [52]. The status of the magnets was continuously monitored and logged [47].

The detector packages were located in well-shielded detector huts built on decks located above each spectrometer (approximately 25 m from the target and 15 m above the floor of the Hall). The bulk of the instrumentation electronics was also located in these huts, and operated remotely from the Counting House. The HRS<sub>e</sub> detector package consisted of a pair of thin scintillator planes [53] used to create triggers, a Vertical Drift Chamber (VDC) package [54, 55] used for particle tracking, and a Gas Čerenkov counter [56] used to distinguish between  $\pi^$ and electron events. Identical elements, except for the Gas Čerenkov counter, were also present in the HRS<sub>b</sub> detector package. The status of the various detector subsystems was continuously monitored and logged [47]. The individual operating efficiencies of each of these three devices was >99%.

#### D. Electronics and data acquisition

For a given spectrometer, a coincidence between signals from the two trigger scintillator planes indicated a 'single-arm' event. Simultaneous  $HRS_e$  and  $HRS_h$  singles events were recorded as 'coincidence' events. The basic trigger logic [57] allowed a prescaled fraction of singlearm events to be written to the data stream. Enough  $HRS_e$  singles were taken for a 1% statistics  ${}^1H(e,e)$  cross section measurement at each kinematics (see Figure 4). Each spectrometer had its own VME crate (for scalers) and FASTBUS crate (for ADCs and TDCs). The crates were managed by readout controllers (ROCs). In addition to overseeing the state of the run, a trigger supervisor (TS) generated the triggers which caused the ROCs to read out the crates on an event-by-event basis. The VME (scaler) crate was also read out every ten seconds. An event builder (EB) collected the resulting data shards into events. An analyzer/data distributer (ANA/DD) analyzed and/or sent these events to the disk of the data

acquisition computer. The entire data acquistion system was managed using the software toolkit CODA [58].

Typical scaler events were about 0.5 kb in length. Typical single-arm events were also about 0.5 kb, while typical coincidence events were about 1.0 kb. The acquisition deadtime  $\eta$  was monitored by measuring the TS output-to-input ratio for each event type. The event rates were set by varying the prescale factors and the beam current such that the DAQ computer was busy at the most only 20% of the time. This resulted in a relatively low event rate (kHz), at which the electronics deadtime was <1%. Online analyzers [59] were used to monitor the quality of the data as it was taken. Eventually, the data were transferred to magnetic tape. The ultimate data analysis was performed on a LINUX CPU farm [60] at the Massachusetts Institute of Technology using the analysis package ESPACE [61].

## III. ANALYSIS

The interested reader is directed to the Ph.D. theses of Gao [62] and Liyanage [63] for a complete discussion of the data analysis. For the sake of completeness, a subset of the aforementioned information is presented here.

## A. Timing corrections and particle identification

Identification of coincidence (e, e'p) events was in general a straightforward process. Software corrections were applied to remove timing variations induced by the trigger scintillator circuit and thus sharpen all Time-of-Flight (ToF) peaks. These included corrections to proton flight times due to variations in the proton kinetic energies, and corrections for variations in the electron and proton path lengths through the spectrometers. Pion rejection was performed using a ToF cut for  $\pi^+$ s in the  $HRS_h$  and the Gas Čerenkov for  $\pi^-$ s in the  $HRS_e$ . A sharp, clear coincidence ToF peak with a FWHM of 1.8 ns and a typical signal-to-noise ratio of 8:1 resulted (see Figure 3). High-energy correlated protons which punched through the  $HRS_h$  collimator (<10% of the prompt yield) were rejected by requiring both spectrometers to independently reconstruct the coincidence-event vertex in the vicinity of the same water film. The resulting promptpeak yields for each water film were corrected for uncorrelated (random) events present in the peak timing region on a bin-by-bin basis (see Owens [64]). These per-film yields were then normalized individually.

## B. Normalization

The relative focal-plane efficiencies for each of the two spectrometers were measured independently for each of the three water films at every spectrometer excitation used in the experiment. By measuring the same

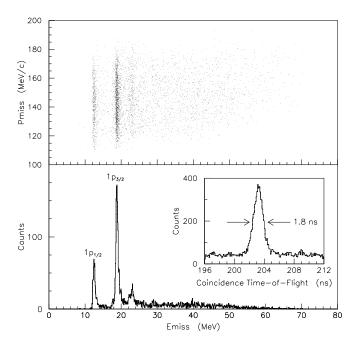


FIG. 3: Yield spectrum obtained at  $E_{\text{beam}} = 0.843 \text{ GeV}$  and  $\theta_{pq} = +8^{\circ}$ , corresponding to  $P_{\rm miss} \approx 148 \ {\rm MeV}/c$ ). Pion rejection has been performed, and all timing corrections have been applied. The top panel shows a scatterplot of  $P_{\text{miss}}$  versus  $E_{\rm miss}$ . The dark vertical bands project into the peaks located at 12.1 and 18.3 MeV in the bottom panel. These peaks correspond to protons knocked-out of the  $1p_{1/2}$ - and  $1p_{3/2}$ -states of <sup>16</sup>O, respectively. The  $E_{\text{miss}}$  resolution was roughly 0.9 MeV FWHM, which did not allow for separation of the  $2s_{1/2}1d_{5/2}$ -doublet located at  $E_{\text{miss}} = 17.4 \text{ MeV}$  from the  $1p_{3/2}$ -state at 18.3 MeV. The bump located at roughly 23 MeV is a negative-parity doublet which was not investigated. The insert shows the corresponding optimized coincidence Time-of-Flight (ToF) peak which has a FWHM of 1.8 ns. The signal-to-noise ratio was about 8:1 in these kinematics.

single-arm cross section at different positions across the spectrometer focal planes, variations in the relative efficiencies were identified. The position variation across the focal plane was investigated by systematically shifting the central excitation of the spectrometer about the mean momentum setting in a series of discrete steps such that the full momentum acceptance was mapped. A smooth, slowly varying dip-region cross section was used instead of a single discrete peak for continuous coverage of the focal plane. The relative-efficiency profiles were unfolded from these data using the program REL-EFF [65] by Weinstein. For each water film, solid-angle cuts were then applied to select the flat regions of the angular acceptance. These cuts reduced the spectrometer apertures by roughly 20% to about 4.8 msr. Finally, relative-momentum cuts were applied to select the flat regions of momentum acceptance. These cuts reduced the spectrometer momentum acceptance by roughly 22% to  $-3.7\% < \delta < 3.3\%$ . The resulting acceptance profile of each spectrometer was uniform to within 1%.

The absolute efficiency at which the two spectrometers operated in coincidence mode was given by

$$\epsilon = \epsilon_e \cdot \epsilon_p \cdot \epsilon_{\text{coin}},\tag{1}$$

where  $\epsilon_e$  was the single-arm HRS<sub>e</sub> efficiency,  $\epsilon_p$  was the single-arm HRS<sub>h</sub> efficiency, and  $\epsilon_{\text{coin}}$  was the coincidencetrigger efficiency. The quantity  $(\epsilon_p \cdot \epsilon_{\rm coin})$  was measured in parallel kinematics at  $E_{\rm beam}=0.843$  GeV using the  ${}^{1}\mathrm{H}(e,e)$  reaction. A 0.7 msr collimator was placed in front of the  $HRS_e$ . In these kinematics, the cone of recoil protons fit entirely into the central flat-acceptance region of the  $HRS_h$ . The number of  ${}^{1}H(e,e)$  events where the proton was detected was compared to the number of  ${}^{1}\mathrm{H}(e,e)$  events where it was not to yield a product of efficiencies ( $\epsilon_p \cdot \epsilon_{\text{coin}}$ ) of 98.9%. The 1.1% effect was due to proton absorption in the waterfall target exit windows, spectrometer windows, and the first layer of trigger scintillators. Since the central field of the  $HRS_h$  was held constant throughout the entire experiment, this measurement was applicable to each of the hadron kinematics employed. A similar method was used to determine the quantity  $(\epsilon_e \cdot \epsilon_{\text{coin}})$  at each of the three HRS<sub>e</sub> field settings. Instead of a collimator, software cuts applied to the recoil protons were used to ensure that the cone of scattered electrons fit entirely into the central flat-acceptance region of the  $HRS_e$ . This product of efficiencies was >99%. Thus, the coincidence efficiency  $\epsilon_{\rm coin}$  was firmly established at nearly 100%. A nominal systematic uncertainty of  $\pm 1.5\%$  was attributed to  $\epsilon$ .

The quantity  $(\ell \cdot \epsilon_e)$ , where  $\ell$  is the luminosity (the product of the effective target thickness and the number of incident electrons) was determined to  $\pm 4\%$  by comparing the measured  ${}^1{\rm H}(e,e)$  cross section for each film at each of the electron kinematics to a parametrization established at a similar  $Q^2$  by Simon et al. [66] and Price et al. [67] (see Figure 4). The results reported in this paper have all been normalized in this fashion. As a consistency check, direct absolute calculation of  $(\ell \cdot \epsilon_e)$  using information from the BCMs, the calibrated thicknesses of the water films, and the single-arm HRS<sub>e</sub> efficiency agrees within uncertainty.

At every kinematics, a Monte Carlo of the phase-space volume subtended by each experimental bin was performed. For each water foil,  $N_0$  software (e,e'p) events were generated, uniformly distributed over the scattered-electron and knocked-out proton momenta  $(p_e, p_p)$  and in-plane and out-of-plane angles  $(\phi_e, \theta_e, \phi_p, \theta_p)$ . For each of these events, all of the kinematic quantities were calculated. The flat-acceptance cuts determined in the analysis of the relative focal-plane efficiency data were then applied, as were all other cuts that had been performed on the actual data. The pristine detection volume  $\Delta V_b(E_{\rm miss}, P_{\rm miss}, \omega, Q^2)$  subtended by a bin  $b(\Delta E_{\rm miss}, \Delta P_{\rm miss}, \Delta \omega, \Delta Q^2)$  containing  $N_b$  pseudoevents was thus

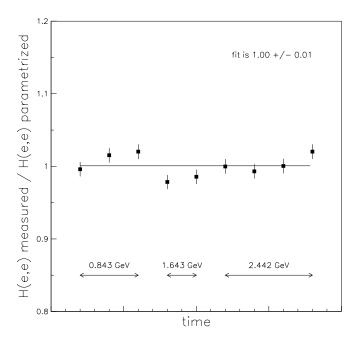


FIG. 4: Measured  ${}^{1}\text{H}(e,e)$  cross sections normalized to the absolute predictions of a parametrization at similiar  $Q^{2}$ . Statistical error bars are shown. The data shown in the figure were taken over the course of a three-month run period. The different data points for each  $E_{\text{beam}}$  represent different HRS<sub>e</sub> angular settings.

$$\Delta V_b(E_{\rm miss}, P_{\rm miss}, \omega, Q^2) = \frac{N_b}{N_0} \left[ (\Delta p_e \cdot \Delta \Omega_e) \cdot (\Delta p_p \cdot \Delta \Omega_p) \right], \quad (2)$$

where the quantity  $(\Delta p_e \cdot \Delta \Omega_e) \cdot (\Delta p_p \cdot \Delta \Omega_p)$  was the total volume sampled over in the Monte Carlo (purposely set larger than the experimental acceptance in all dimensions) [129]. The pseudodata were binned exactly as the real data, and uniformly on both sides of  $\vec{q}$ . At each kinematics, the bin with the largest volume  $\Delta V_{\rm max}$  was located. Only bins subtending volumes larger than 50% of  $\Delta V_{\rm max}$  were analyzed further.

Corrections based on the TS output-to-input ratio were applied to the data to account for the acquisition deadtime to coincidence events. On average, these corrections were roughly 20%. An acquisition Monte Carlo by Liang [68] was used to cross-check these corrections and establish the absolute uncertainty in them at 2%.

Corrections to the per-film cross sections for electron radiation before and after scattering were calculated on a bin-by-bin basis in two ways: first using a version of the code RADCOR by Quint [69] modified by Florizone [70], and independently, the prescriptions of Borie and Dreschel [71] modified by Templon  $et\ al.$  [72] for use within the simulation package MCEEP by Ulmer [73]. The two approaches agreed to within the statistical uncertainty of the data and amounted to <55% of the measured cross section for the bound states, and <15% of the measured cross section for the continuum. Corrections for proton radiation at these energies are much less than 1% and were not performed.

## C. Cross sections

The radiatively corrected average cross section in the bin  $b(\Delta E_{\rm miss},\,\Delta P_{\rm miss},\,\Delta\omega,\,\Delta Q^2)$  was calculated according to

$$\left\langle \frac{d^{6}\sigma}{d\omega \ d\Omega_{e} \ dE_{\text{miss}} \ d\Omega_{p}} \right\rangle_{b} = \frac{R_{^{16}\text{O}(e,e'p)}}{(\ell \cdot \epsilon_{e})(\epsilon_{p} \cdot \epsilon_{\text{coin}})} \left(\frac{Y_{b}}{\Delta V_{b}}\right), \quad (3)$$

where  $Y_b$  was the total number of real events which were detected in  $b(\Delta E_{\text{miss}}, \Delta P_{\text{miss}}, \Delta \omega, \Delta Q^2), (\ell \cdot \epsilon_e)$  was determined from the ratio of the measured  ${}^{1}\mathrm{H}(e,e)$  cross section to the parametrized cross section,  $(\epsilon_p \cdot \epsilon_{\text{coin}})$  was the product of the proton and coincidence detection efficiency,  $\Delta V_b$  was the phase-space volume, and  $R_{^{16}\text{O}(e,e'p)}$ was a correction applied to account for events which radiated in or out of  $\Delta V_b$ . The average cross section was calculated as a function of  $E_{\text{miss}}$  for a given kinematic setting [130]. Bound-state cross sections for the 1p-shell were extracted by integrating over the appropriate range in  $E_{\text{miss}}$ , weighting with the appropriate Jacobian [131]. Five-fold differential cross sections for QE proton knockout from the 1p-shell of <sup>16</sup>O are presented in Tables XI and XII. Six-fold differential cross sections for QE proton knockout from  $^{16}$ O at higher  $E_{\text{miss}}$  are presented in Tables XIII - XXII.

## D. Asymmetries and response functions

In the first Born (one-photon exchange) approximation, the unpolarized six-fold differential cross section may be expressed in terms of four independent effective response functions as [2, 8, 74]

$$\frac{d^6\sigma}{d\omega \ d\Omega_e \ dE_{\text{miss}} \ d\Omega_p} = K \ \sigma_{\text{Mott}} \left[ v_L R_L + v_T R_T + v_{LT} R_{LT} \cos(\phi) + v_{TT} R_{TT} \cos(2\phi) \right], \tag{4}$$

where K is a kinematic factor,  $\sigma_{\mathrm{Mott}}$  is the Mott cross section, and the  $v_{\mathrm{i}}$  are dimensionless kinematic factors [132]. Ideal response functions are not directly measureable because electron distortion does not permit the azimuthal dependences to be separated exactly. The effective response functions which are extracted by applying Equation (4) to the data are denoted  $R_L$  (longitudinal),  $R_T$  (transverse),  $R_{LT}$  (longitudinal-transverse), and  $R_{TT}$  (transverse-transverse). They contain all the information which may be extracted from the hadronic system using (e,e'p). Note that the  $v_{\mathrm{i}}$  depend only on  $(\omega,Q^2)$ , while the response functions depend on  $(\omega,Q^2,E_{\mathrm{miss}},P_{\mathrm{miss}})$ .

The individual contributions of the response functions may be separated by performing a series of cross section measurements varying  $v_i$  and/or  $\phi$ , but keeping  $\vec{q}$  and  $\omega$ constant [133]. In the case where the proton is knockedout of the nucleus in a direction parallel to  $\vec{q}$  (parallel kinematics), the interference terms  $R_{LT}$  and  $R_{TT}$  vanish, and a Rosenbluth separation [75] may be performed to separate  $R_L$  and  $R_T$ . In the case where the proton is knocked-out of the nucleus in the scattering plane with a finite angle  $\theta_{pq}$  with respect to  $\vec{q}$  (quasi-perpendicular kinematics), the asymmetry  $A_{LT}$  and the interference  $R_{LT}$  may be separated by performing symmetric cross section measurements on either side of  $\vec{q}$  ( $\phi = 0^{\circ}$  and  $\phi = 180^{\circ}$ ). The contribution of  $R_{TT}$  cannot be separated from that of  $R_L$  with only in-plane measurements; however, by combining the two techniques, an interesting combination of response functions  $R_T$ ,  $R_{LT}$ , and  $R_{L+TT}$ [134] may be extracted.

For these data, response function separations were performed where the phase-space overlap between kinematics permitted. For these separations, bins were selected only if their phase-space volumes  $\Delta V_b$  were all simultaneously 50% of  $\Delta V_{\rm max}$ . Separated response functions for QE proton knockout from the 1p-shell <sup>16</sup>O are presented in Tables XXIII, XXIV, and XXV. Separated response functions for QE proton knockout from the <sup>16</sup>O continuum are presented in Tables XXVI, XXVII, and XXVIII.

## E. Systematic uncertainties

The systematic uncertainties in the cross-section measurements were classified into two categories – kinematic-dependent uncertainies and scale uncertainties. For a complete discussion of how these uncertainties were evaluated, the interested reader is directed to a report by Fissum and Ulmer [76]. For the sake of completeness, a subset of the aforementioned information is presented here.

In a series of simulations performed after the experiment, MCEEP was used to investigate the intrinsic behavior of the cross-section data when constituent kinematic parameters were varied over the appropriate experimentally determined ranges presented in Table III. Based on the experimental data, the high- $E_{\rm miss}$  region was modelled as the superposition of a peak-like  $1s_{1/2}$ -

TABLE III: Kinematic-dependent systematic uncertainties folded into the MCEEP simulation series.

| Quantity            | description                           | δ                    |
|---------------------|---------------------------------------|----------------------|
| $E_{\mathrm{beam}}$ | beam energy                           |                      |
| $\phi_{ m beam}$    | in-plane beam angle                   | $ignored^a$          |
| $	heta_{ m beam}$   | out-of-plane beam angle               | $2.0 \mathrm{\ mr}$  |
| $p_e$               | scattered electron momentum           | $1.5 \times 10^{-3}$ |
| $\phi_e$            | in-plane scattered electron angle     | $0.3 \mathrm{\ mr}$  |
| $	heta_e$           | out-of-plane scattered electron angle | $2.0 \mathrm{\ mr}$  |
| $p_p$               | proton momentum                       | $1.5 \times 10^{-3}$ |
| $\phi_p$            | in-plane proton angle                 | $0.3 \mathrm{\ mr}$  |
| $\theta_p$          | out-of-plane proton angle             | 2.0 mr               |

 $^a$ The angle of incidence of the electron beam was determined using a pair of beam position monitors (BPMs) located upstream of the target (see Figure 2). The BPM readback was calibrated by comparing the location of survey fiducials along the beamline to the Hall A survey fiducials. Thus, in principle, uncertainty in the knowledge of the incident electron-beam angle should be included in this analysis. However, the simultaneous measurement of the kinematically overdetermined  $^1{\rm H}(e,ep)$  reaction allowed for a calibration of the absolute kinematics, and thus an elimination of this uncertainty. That is, the direction of the beam defined the axis relative to which all angles were measured via  $^1{\rm H}(e,ep)$ .

state on a flat continuum. Contributions to the systematic uncertainty from this flat continuum were taken to be small, leaving only those from the  $1s_{1/2}$ -state. The  $^{16}{\rm O}(e,e'p)$  simulations incorporated as physics input the bound-state RDWIA calculations detailed in Section IV A, which were based on the experimental 1p-shell data.

For each kinematics, the central water foil was considered, and 1M events were generated. In evaluating the simulation results, the exact cuts applied in the actual data analyses were applied to the pseudo-data, and the cross sections were evaluated for the identical  $P_{\text{miss}}$ bins used to present the results. The experimental constraints to the kinematic-dependent observables afforded by the overdetermined  ${}^{1}\mathrm{H}(e,ep)$  reaction were exploited to calibrate or constrain the experimental setup. The inplane electron and proton angles  $\phi_e$  and  $\phi_p$  were chosen as independent parameters. When a known shift in  $\phi_e$ was made,  $\phi_p$  was held constant and the complementary variables  $E_{\text{beam}}$ ,  $p_e$ , and  $p_p$  were varied as required by the constraints enforced by the  ${}^{1}\mathrm{H}(e,ep)$  reaction. Similarly, when a known shift in  $\phi_p$  was made,  $\phi_e$  was held constant and the complementary variables  $E_{\text{beam}}$ ,  $p_e$ , and  $p_p$  were varied as appropriate. The overall constrained uncertainty was taken to be the quadratic sum of the two contributions.

The global convergence of the uncertainty estimate was examined for certain extreme kinematics, where 10M-event simulations (which demonstrated the same behavior) were performed. The behavior of the uncertainty as a function of  $P_{\rm miss}$  was also investigated by examining the uncertainty in the momentum bins adjacent to the reported momentum bin in exactly the same fashion. The kinematically induced systematic uncertainty in the  $^{16}{\rm O}(e,e'p)$  cross sections was determined to be de-

pendent upon  $P_{\text{miss}}$ , with an average value of 1.4%. The corresponding uncertainties in the  ${}^{1}\text{H}(e,e)$  cross sections were determined to be negligible.

The scale systematic uncertainties which affect each of the cross-section measurements are presented in Table IV. As previously mentioned, the  $^{16}\text{O}(e,e'p)$  cross-section results reported in this paper have been normalized by comparing simultaneously measured  $^{1}\text{H}(e,e)$  cross sections to a parametrization established at a similar  $Q^2$  [66, 67]. Thus, the first seven listed uncertainties simply divide out of the quotient, such that only the subsequent uncertainties affect our results. The average systematic uncertainty associated with a 1p-shell cross section was 5.6%, while that for the continuum was 5.9%. The small difference was due to contamination of the high- $E_{\text{miss}}$  data by collimator punch-through events.

The quality of these data in terms of their associated systematic uncertainties was clearly demonstrated by the results obtained for the response-function separations. In Figure 5, cross sections measured in parallel kinematics at three different beam energies as a function of the separation lever arm  $v_T/v_L$  for the 1p-shell are shown. The values of the response functions  $R_L$  (offset) and  $R_T$ (slope) were extracted from the fitted line. The extremely linear trend in the data indicated that the magnitude of the systematic uncertainties was small, and that statistical uncertainties dominated. This is not simply a test of the one-photon exchange approximation employed in the data analysis as it has been demonstrated by Traini et al. [77] and Udías [78] that the linear behavior of the Rosenbluth plot persists even after Coulomb distortion is included.

Given the applicability of the one-photon exchange approximation at these energies, the quality of the data was also demonstrated by the results extracted from identical measurements which were performed in different electron kinematics. The asymmetries  $A_{LT}$  and response functions  $R_{LT}$  for QE proton knockout were extracted for both  $E_{\rm beam}=1.643~{\rm GeV}$  and 2.442 GeV for  $\theta_{pq}=\pm 8^{\circ}$  ( $P_{\rm miss}\approx 148~{\rm MeV}/c$ ). They agree within the statistical uncertainty. Table XXV presents the results at both beam energies for 1p-shell knockout for  $< Q^2>=0.800~{\rm (GeV}/c)^2, <\omega>=436~{\rm MeV},$  and  $< T_p>=427~{\rm MeV},$  while Figure 6 shows the results for 25 MeV  $< E_{\rm miss}<60~{\rm MeV}$ . The excellent agreement of these values indicates that the systematic uncertainties were much smaller than the statistical uncertainties.

## IV. THEORETICAL OVERVIEW

In the following subsections, brief overviews of the Relativistic Distorted-Wave Impulse Approximation (RDWIA), Relativistic Optical-Model Eikonal Approximation (ROMEA), and Relativistic Multiple-Scattering Glauber Approximation (RMSGA) calculations are presented.

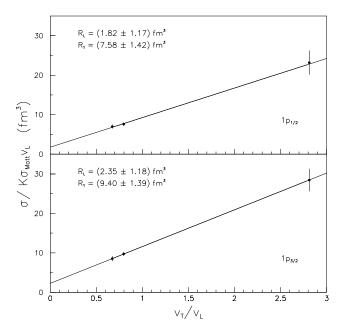


FIG. 5: Cross sections for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  measured in parallel kinematics at three different beam energies as a function of the separation lever arm  $v_T/v_L$ . The data points correspond to beam energies of 2.442, 1.643, and 0.843 GeV from left to right. The response functions  $R_L$  (offset) and  $R_T$  (slope) have been extracted from the fitted line. The uncertainties shown are statistical only. The extremely linear behavior of the data (which persists even after corrections for Coulomb distortion are applied) indicates the systematic uncertainties were dominated by statistical uncertainties (see Section III E for a complete discussion).

## A. RDWIA

In RDWIA, the interaction is described within the constraints of the Impulse Approximation (IA). It is thus assumed that the exchange photon interacted with a single target nucleon, and that nucleon is subsequently detected. With these assumptions, the relevant quantity is the one-body nucleon current given in momentum space by Picklesimer and Van Orden [7, 8] and subsequently by Udías et al. [15] as

$$J_N^{\mu}(\omega, \vec{q}) = \int d\vec{p} \; \bar{\psi}_F(\vec{p} + \vec{q}) \; \hat{j}_N^{\mu}(\omega, \vec{q}) \; \psi_B(\vec{p}) \; . \tag{5}$$

 $\psi_B$  represents the overlap between the initial target nucleus and the residual nucleus. In practice, this overlap is approximated by a single-particle bound-state solution of a mean-field potential for the initial nucleus, with quantum numbers corresponding to the resulting hole corresponding to the knocked-out proton.  $\psi_F$  is the wave function of the knocked-out (and detected) nucleon. The interaction between this nucleon and the residual nucleus in

TABLE IV: Summary of the scale systematic uncertainties contributing to the cross-section measurements. The first seven entries do not contribute to the systematic uncertainties in the reported cross sections as they contribute equally to the  ${}^{1}\text{H}(e,e)$  cross sections to which the  ${}^{16}\text{O}(e,e'p)$  are normalized.

| Quantity   | description   | δ (%) |
|--|---|-------|
| $\eta_{ m DAQ}$  | data acquisition deadtime correction                                | 2.0   |
| $\eta_{ m elec}$   | electronics deadtime correction                                     | <1.0  |
| ho t'  | effective target thickness  | 2.5   |
| $N_e$  | number of incident electrons  | 2.0   |
| $\epsilon_e$   | electron dectection efficiency                                      | 1.0   |
| $\Delta\Omega_e{}^a$   | $\mathrm{HRS}_e$ solid angle  | 2.0   |
| $\epsilon_e \cdot \epsilon_p \cdot \epsilon_{\mathrm{coin}}$                   | product of electron, proton, and coincidence efficiencies           | 1.5   |
| $\ell \cdot \epsilon_e$  | obtained from a form factor parametrization of ${}^{1}{\rm H}(e,e)$ | 4.0   |
| $\frac{\ell \cdot \epsilon_e}{R_{^{16}O(e,e'p)}^{b}}^{b}$ $R_{^{1}H(e,e)}^{b}$ | radiative correction to the ${}^{16}{\rm O}(e,e'p)$ data            | 2.0   |
| $R_{^{1}\mathrm{H}(e,e)}{^{b}}$  | radiative correction to the ${}^{1}\mathrm{H}(e,e)$ data            | 2.0   |
| $\epsilon_p \cdot \epsilon_{ m coin}$  | product of proton and coincidence efficiencies                      | <1.0  |
| $\Delta\Omega_p{}^a$   | $HRS_h$ solid angle   | 2.0   |
| punchthrough   | protons which punched through the ${ m HRS}_h$ collimator           | 2.0   |

<sup>a</sup>The systematic uncertainties in the solid angles  $\Delta\Omega_e$  and  $\Delta\Omega_p$  were quantified by studying sieve-slit collimator optics data at each of the spectrometer central momenta employed. The angular locations of each of the reconstructed peaks corresponding to the 7 × 7 lattice of holes in the sieve-slit plate were compared to the locations predicted by spectrometer surveys, and the overall uncertainty was taken to be the quadratic sum of the individual uncertainties.

 $^b$ At first glance, it may be surprising to note that the uncertainty due to the radiative correction to the data is included as a scale uncertainty. In general, the radiative correction is strongly dependent on kinematics. However, the 1p-shell data analysis, and for that matter any bound-state data analysis, involves  $E_{\rm miss}$  cuts. These cuts to a large extent remove the strong kinematic dependence of the radiative correction, since only relatively small photon energies are involved. In order to compensate for any remaining weak kinematic dependence, the uncertainty due to the radiative correction was slightly overestimated.

<sup>c</sup>High  $E_{\text{miss}}$  data only.

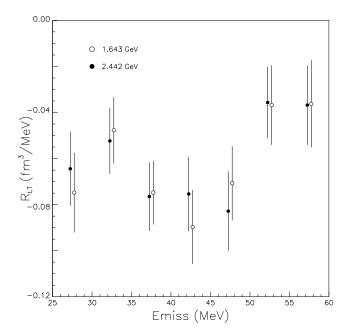


FIG. 6:  $R_{LT}$  for  $\theta_{pq}=\pm 8^\circ$  ( $P_{\rm miss}\approx 145~{\rm MeV/}c$ ) as a function of  $E_{\rm miss}$  for  $E_{\rm beam}=1.643~{\rm GeV}$  and 2.442 GeV. Statistical uncertainties only are shown. The statistical agreement over a broad range of  $E_{\rm miss}$  emphasizes the systematic precision of the measurement (see Section III E for a complete discussion). Note that the averages of these  $R_{LT}$  values are presented as the  $P_{\rm miss}\approx 145~{\rm MeV/}c$  data in Figure 24 and Table XXVIII.

the final state is taken into account by means of an optical potential adjusted to reproduce proton-scattering data over the energy range of interest. In the relativistic formalism,  $\psi_B$  and  $\psi_F$  are relativistic wave functions. Further, a relativistic single-nucleon current operator,  $\hat{j}_N^{\mu}$ , is employed.

In (5), the relativistic bound-nucleon wave function  $\psi_B$  is a four-spinor with well-defined angular momentum quantum numbers  $\kappa$  and  $\mu$  corresponding to the particular shell under consideration. In coordinate space, this wave function is given by

$$\psi_{\kappa}^{\mu}(\vec{r}) = \begin{pmatrix} g_{\kappa}(r) \ \phi_{\kappa}^{\mu}(\hat{r}) \\ if_{\kappa}(r) \ \phi_{-\kappa}^{\mu}(\hat{r}) \end{pmatrix} , \qquad (6)$$

which is a total angular momentum eigenstate with eigenvalue  $j=|\kappa|-1/2;$  that is,

$$\phi_{\kappa}^{\mu}(\hat{r}) = \sum_{m,\sigma} \langle l \ m \ \frac{1}{2} \ \sigma | j \ \mu \rangle \ Y_{lm}(\hat{r}) \ \chi_{\sigma}^{\frac{1}{2}}$$
 (7)

with  $l = \kappa$  if  $\kappa > 0$  and  $l = -\kappa - 1$  if  $\kappa < 0$ . The functions  $f_{\kappa}$  and  $g_{\kappa}$  satisfy the usual coupled linear differential equations [15, 79–81].

The relativistic mean-field potentials employed may be derived as by Horowitz *et al.* [82] from a relativistic Lagrangian with  $\sigma$ ,  $\omega$ ,  $\rho$ , and  $\gamma$  exchanges, using the NLSH parameters of Sharma *et al.* [83] The wave function for the outgoing proton,  $\psi_F$ , is a scattering solution of the

Dirac equation, which includes S–V global optical potentials. This wave function has been obtained as a partial wave expansion in configuration space by Udías *et al.* as [15, 17]

$$\psi_F(\vec{r}) = 4\pi \sqrt{\frac{E_F + M}{2E_F V}} \cdot \sum_{\kappa,\mu,m} e^{-i\delta_{\kappa}^* i^l \langle l \ m \ \frac{1}{2} \ \sigma_F | j \ \mu \rangle} Y_{lm}^*(\hat{P}_F) \ \psi_{\kappa}^{\mu}(\vec{r}) \ , \ (8)$$

where the  $\psi_{\kappa}^{\mu}(\vec{r})$  are four-spinors of the form given in (6). The phase-shifts and radial functions are complex because of the complex potential. For the scattered-proton wave function, amongst other choices, the Energy-Dependent A-independent potential for <sup>16</sup>O EDAI-O derived by Cooper et al. [84] may be used.

As discussed by Udías et al. [15] and Caballero et al. [85, 86], the choice of the current operator  $\hat{j}^{\mu}$  is to some extent arbitrary. As per de Forest [87] and Kelly [3, 88, 89], three expressions for CC may be considered

$$\hat{j}_{cc1}^{\mu} = G_M(Q^2)\gamma^{\mu} - \frac{\kappa}{2M}F_2(Q^2)\overline{P}^{\mu} , 
\hat{j}_{cc2}^{\mu} = F_1(Q^2)\gamma^{\mu} + i\frac{\kappa}{2M}F_2(Q^2)\sigma^{\mu\nu}q_{\nu} , 
\hat{j}_{cc3}^{\mu} = F_1(Q^2)\frac{\overline{P}^{\mu}}{2M} + \frac{i}{2M}G_M(Q^2)\sigma^{\mu\nu}q_{\nu} ,$$
(9)

where  $q^{\mu}=(\vec{q},\omega)$  is the four-momentum transfer,  $Q^2=\vec{q}^2-\omega^2$ ,  $\overline{P}^{\mu}=(E+E',\vec{p}+\vec{p}')$ ,  $\kappa$  is the anomalous part of the magnetic moment,  $F_1$  and  $F_2$  are the Dirac and Pauli nucleon form factors,  $G_M=F_1+\kappa F_2$  is the Sachs nucleon magnetic form factor, and  $\sigma^{\mu\nu}=i/2\left[\gamma^{\mu},\gamma^{\nu}\right]$ .

When comparing RDWIA with nonrelativistic approaches (NRDWIA), dynamical effects due to the differences between relativistic and nonrelativistic wave functions arise. Salient features of these dynamical effects are a depression of the upper component of the scatterednucleon wave function in the nuclear interior (typically identified as by Udías et al. [17] as the effect of the Darwin term coming from the derivative of the optical S-V potentials), and an enhancement of the lower components, mainly those of the bound-nucleon wave function. The effect caused by the nonlocal Darwin term was studied in detail for <sup>40</sup>Ca and <sup>208</sup>Pb by Udías et al. [15, 17]. It causes an apparent enhanced absorption when comparing the RDWIA and DWIA differential cross sections at moderate  $P_{\text{miss}}$  values, and thus the normalization factors derived in RDWIA are larger, as shown by Udías et al. [15, 17], McDermott [90], and Jin et al. [91]. The effect of the dynamical enhancement of the lower components was studied by Caballero et al. [18, 86] in RPWIA. It was also studied in RDWIA by Udías et al. [19] at high  $Q^2$ . In both cases, it was found to play a crucial role in the  $R_{LT}$  responses.

Figure 7 illustrates comparisons between RPWIA and RDWIA calculations by Kelly (LEA) for the kinematics

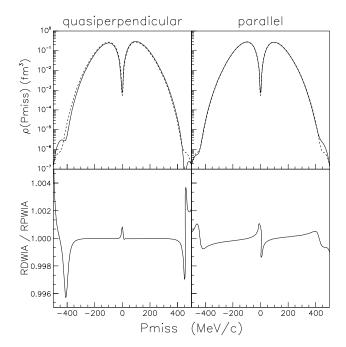


FIG. 7: Comparisons between RPWIA and RDWIA calculations for the removal of protons from the  $1p_{1/2}$ -state of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442~{\rm GeV}.$  In the upper panels, the solid curves represent the reduced cross sections for both the IA calculations (see text for details), while the dashed curves correspond to the momentum distributions. In the lower panels, the (RDWIA / RPWIA) reduced cross-section ratio is shown. Agreement to much better than 1% is obtained for both kinematics over the entire  $P_{\rm miss}$  range.

of this experiment for the removal of protons from the  $1p_{1/2}$ -state of <sup>16</sup>O as a function of  $P_{\text{miss}}$  for  $E_{\text{beam}} =$ 2.442 GeV. In the upper panels, the solid curves represent the reduced cross sections for both the IA calculations as the difference between them is too small to notice on this scale. The dashed curves correspond to the momentum distributions. The RPWIA reduced cross sections clearly remain close to the momentum distributions except in the vicinities of the nodes, and thus the violation of factorization is rather mild. In the lower panels, the (RDWIA / RPWIA) reduced cross-section ratio is shown. The RDWIA calculations employ a standard partial-wave expansion of the second-order Dirac equation with optical and Coulomb potentials nullified, and use a target mass  $M_A = 1601 m_p$  to minimize recoil corrections and frame ambiguities. The RPWIA calculations do not solve the Dirac equation, but rather employ a simpler integral instead. Agreement to much better than 1\% is obtained for both kinematics over the entire  $P_{\text{miss}}$  range, which indicates that the partial-wave expansion of the secondorder version of the Dirac equation is very accurate for plane waves.

Figures 8 and 9 illustrate the agreement between independent RDWIA calculations (hereafter referred to as

TABLE V: A summary of the basic RDWIA options which served as input to the "baseline" calculations of the Madrid Group and Kelly. See Section V for further details.

| Innut Danamatan           | Option             |
|---------------------------|--------------------|
| Input Parameter           | Ориоп              |
| bound-state wave function | NLSH               |
| Optical Model             | EDAI-O             |
| nucleon spinor distortion | fully relativistic |
| electron distortion       | none               |
| current operator          | CC2                |
| nucleon form factors      | dipole             |
| gauge                     | Coulomb            |

"baseline") performed by the Madrid Group [92] and Kelly [93] when identical basic input options are chosen. These options are summarized in Table V. Note that they do *not* represent the best physics choice of the various inputs; rather, they were selected to simplify the comparison between the two calculational frameworks. See Section V for further details.

Figure 8 shows "baseline" calculations by the Madrid Group and Kelly (LEA) for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Cross sections are shown in the top panel, while the ratios of the cross sections are shown in the bottom panel. Differences between the two calculations amount to less than 2% for  $|P_{\rm miss}|<250~{\rm MeV}/c$ , but become appreciable for larger  $|P_{\rm miss}|$ . The somewhat sharp deviation between the two calculations for  $|P_{\rm miss}|>300~{\rm MeV}/c$  persists regardless of the set of input parameters chosen for the "baseline" comparisons.

Figure 9 shows "baseline" calculations for the  $A_{LT}$  asymmetry by the Madrid Group and Kelly (LEA) for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Despite the effects illustrated in Figure 8 at  $|P_{\rm miss}|>300~{\rm MeV}/c,~A_{LT}$  extracted from the two calculations is essentially identical (other than a very slight phase offset). Kelly concludes that since  $A_{LT}$  is very sensitive to spinor distortion and the details of the current operator, these aspects of the two RDWIA calculations are in very good agreement.

## B. ROMEA / RMSGA

In this subsection, an alternate relativistic model developed by the Ghent Group [94–96] for  $A+e\longrightarrow (A-1)+e'+p$  processes is presented. With respect to the construction of the the bound-state wave functions and the nuclear-current operator, an approach similar to standard RDWIA is followed. The major differences lie in the construction of the scattering wave function. Indeed, the approach presented here adopts the relativistic Eikonal Approximation (EA) to determine the scattering wave functions and may be used in conjuction with both the Optical Model and the multiple-scattering Glauber frameworks for dealing with the final-state interactions

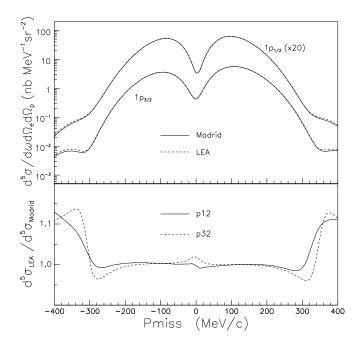


FIG. 8: Baseline RDWIA calculations by the Madrid Group and Kelly (LEA) for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. For the purposes of this comparison, the input into both calculations was identical (see Table V). Overall agreement is very good, and agreement is excellent for  $|P_{\rm miss}|<250~{\rm MeV}/c$ .

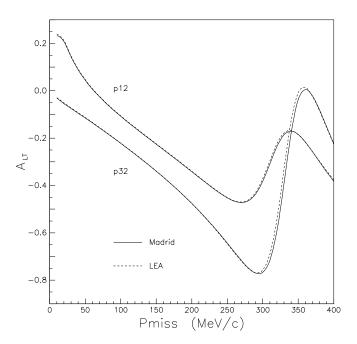


FIG. 9: Baseline RDWIA calculations for the  $A_{LT}$  asymmetry by the Madrid Group and Kelly (LEA) for the removal of protons from the 1*p*-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Overall agreement is excellent over the entire  $P_{\rm miss}$  range.

(FSI).

The EA belongs to the class of semi-classical approximations which are meant to become "exact" in the limit of small de Broglie (db) wavelengths,  $\lambda_{db} \ll a$ , where a is the typical range of the potential in which the particle is moving. For a particle moving in a relativistic (optical) potential consisting of scalar and vector terms, the scattering wave function takes on the following EA form

$$\psi_F(\vec{r}) \sim \left[ \frac{1}{E + M + V_s(\vec{r}) - V_v(\vec{r})} \vec{\sigma} \cdot \vec{p} \right] e^{i\vec{p}_p \cdot \vec{r}} e^{iS(\vec{r})} \chi_{\sigma}^{1/2} . \tag{10}$$

This wave function differs from a relativistic plane wave in two respects: first, there is a dynamical relativistic effect from the scalar  $V_s(\vec{r})$  and vector  $V_v(\vec{r})$  potentials which enhances the contribution from the lower components; and second, the wave function contains an eikonal phase which is determined by integrating the central  $(V_c)$  and spin-orbit  $(V_{so})$  terms of the distorting potentials along the (asymptotic) trajectory of the escaping particle. In practice, this amounts to numerically calculating the integral  $(\vec{r} \equiv (\vec{b}, z))$ 

$$iS(\vec{b},z) = -i\frac{M}{K} \int_{-\infty}^{z} dz' \left[ V_c(\vec{b},z') + V_{so}(\vec{b},z') [\vec{\sigma} \cdot (\vec{b} \times \vec{K}) - iKz'] \right], \quad (11)$$

where  $\vec{K} \equiv \frac{1}{2} (\vec{p}_p + \vec{q})$ .

Within the ROMEA calculation, the eikonal phase (11) is computed from the relativistic optical potentials as they are derived from global fits to elastic proton-nucleus scattering data. For the results presented in this work, EDAI-O is used. It is worth stressing that the sole difference between the ROMEA and the RDWIA models is the use of the EA to compute the scattering wave functions.

For proton lab momenta exceeding 1  $\,\mathrm{GeV}/c$ , the highly inelastic nature of the elementary nucleon-nucleon (NN) scattering process makes the use of a potential method for describing FSI effects artificial. In this high-energy regime, an alternative description of FSI processes is provided by the Glauber Multiple-Scattering Theory. A relativistic and unfactorized formulation of the this theory has been developed by the Ghent Group [96, 97]. In this framework, the A-body wave function in the final state reads

$$\Psi_{A}^{\vec{p}_{p},m_{s}}(\vec{r},\vec{r}_{2},\vec{r}_{3},...\vec{r}_{A}) \sim \widehat{\mathcal{O}}\left[\frac{1}{\frac{1}{E+M}\vec{\sigma}\cdot\vec{p}_{p}}\right]e^{i\vec{p}_{p}\cdot\vec{r}}\chi_{\frac{1}{2}m_{s}} \times \Psi_{A-1}^{J_{R}M_{R}}(\vec{r}_{2},\vec{r}_{3},...\vec{r}_{A}) (12)$$

where  $\Psi_{A-1}^{J_R M_R}$  is the wave function characterizing the state in which the A-1 nucleus is created. In the above expression, the subsequent elastic or "mildly inelastic"

TABLE VI: A summary of the basic ROMEA and RMSGA options which served as input to the calculations of the Ghent Group. See Section V for further details.

| Input Parameter           | Option             |
|---------------------------|--------------------|
| bound-state wave function | [100]              |
| Optical Model             | EDAI-O             |
| nucleon spinor distortion | fully relativistic |
| electron distortion       | none               |
| current operator          | CC2                |
| nucleon form factors      | dipole             |
| gauge                     | Coulomb            |

collisions which the ejectile undergoes with "frozen" spectator nucleons are implemented through the introduction of the operator

$$\widehat{\mathcal{O}}\left(\vec{r}, \vec{r}_{2}, \vec{r}_{3}, \dots \vec{r}_{A}\right) \equiv \prod_{j=2}^{A} \left[1 - \Gamma\left(\mid \vec{p}_{p} \mid, \vec{b} - \vec{b_{j}}\right) \theta\left(z - z_{j}\right)\right] ,$$

where the profile function for pN scattering is

$$\Gamma(p_p, \vec{b}) = \frac{\sigma_{pN}^{tot}(1 - i\epsilon_{pN})}{4\pi\beta_{pN}^2} \exp\left(-\frac{b^2}{2\beta_{pN}^2}\right) .$$

In practice, for the lab momentum of a given ejectile, the following input is required: the total proton-proton and proton-neutron cross sections  $\sigma_{pN}^{tot}$ , the slope parameters  $\beta_{pN}$  and the ratio of the real-to-imaginary scattering amplitude  $\epsilon_{pN}$ . The parameters  $\sigma_{pN}^{tot}$ ,  $\beta_{pN}$ , and  $\epsilon_{pN}$  are obtained through interpolation of the data base made available by the Particle Data Group [98]. The A(e,e'p) results obtained with a scattering state of the form of (12) are referred to as (RMSGA) calculations. It is worth stressing that in contrast to the RDWIA and the ROMEA models, all parameters entering the calculation of the scattering states in RMSGA are directly obtained from the elementary proton-proton and proton-neutron scattering data.

Note that for the kinematics of the  $^{16}{\rm O}(e,e'p)$  experiment presented in this paper, the de Broglie wavelength of the ejected proton is  $\lambda_{db}\approx 0.2$  fm, and thus both the optical potential and the Glauber frameworks may be applicable. Indeed, for  $T_p\approx 0.433$  GeV, various sets of relativistic optical potentials are readily available and according to the Ghent Group [96],  $\lambda_{db}$  appears sufficiently small for the approximations entering the Glauber framework to be justifiable.

The basic ROMEA and RMSGA options which served as input to the calculations of the Ghent Group [99] are presented in Table VI.

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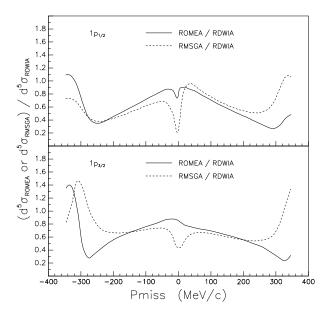


FIG. 10: Suggested to replace this figure with RP-WIA comparison between LEA/Madrid and Ghent or delete it completely: Baseline RDWIA calculations compared to "bare" (no MEC nor IC) ROMEA and RMSGA calculations by the Ghent Group for the removal of protons from the 1p-shell of <sup>16</sup>O as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Overall agreement is reasonable, particularly for  $|P_{\rm miss}|<200~{\rm MeV}/c$ .

calculations of the Ghent Group together with the "baseline" RDWIA calculations for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. The cross-section ratio (ROMEA / RDWIA) is shown in the top panel, while the cross-section ratio (RMSGA / RDWIA) is shown in the bottom panel. While the calculational frameworks and basic ingredients differ between the three approaches, agreement is obviously reasonable (particularly for  $|P_{\rm miss}|<200~{\rm MeV}/c$ ), thus underlining the validity of the EA.

## V. DISCUSSION

The data were interpreted in subsets corresponding to the 1p-shell and the  $1s_{1/2}$ -state and continuum, respectively. The interested reader is directed to the works of Gao  $et\ al.\ [101]$  and Liyanage  $et\ al.\ [102]$ , where these results have been briefly highlighted. A detailed discussion is presented below.

## A. 1p-shell results

In this section, the results for proton removal from the 1p-shell of  $^{16}\mathrm{O}$  are discussed first in terms of single-

nucleon current calculations, and then considering twobody current contributions stemming from MEC and IC.

## 1. Single-nucleon currents

The consistency of the normalization factors  $S_{\alpha}$  suggested by the 1p-shell data obtained from this measurement was studied in detail within the RDWIA framework. One study by Kelly [103] focused on consistency with respect to other  $^{16}{\rm O}(e,e'p)$  data sets (see Table VII) for  $|P_{\rm miss}| \leq 200~{\rm MeV}/c$ . A complementary study by the Madrid Group [104] focused instead on the  $|P_{\rm miss}| \leq 350~{\rm MeV}/c$  data obtained from this work at 2.442 GeV (see Table XII). The studies involved systematically varying a wide range of inputs to the RDWIA calculations, and then performing least-squares fits of the predictions to the cross-section data. The normalization factors thus extracted are presented in Tables VIII and IX.

The consistency analysis employed the Coulomb gauge, the CC2 current operator, the MMD nucleon form-factor model of Mergell et al. [105], and included the effects of electron distortion. Three bound-nucleon wave functions (see Figure 11) derived from relativistic Lagrangians were considered: HS by Horowitz and Serot [82, 106], NLSH, and NLSH-P by Udías et al. [107] (which resulted from a Lagrangian fine-tuned to reproduce data set (a)). When experimentally unresolved, the contamination of the  $1p_{3/2}$ -state doublet was instead computed by incoherently including the parametrizations of Leuschner et al. Note that both the NLSH and NLSH-P wave functions predict binding energies, single-particle energies, and a charge radius for <sup>16</sup>O which are all in good agreement with the data. The optical potential was changed between two purely phenomenological S-V potentials based upon the Dirac equation: EDAI-O and EDAD1 (an energydependent, atomic-mass dependent parametrization for many nuclei by Cooper et al. [84]).

Qualitatively, the calculations which employed the HS and NLSH-P bound-nucleon wave functions fitted the low  $Q^2$  data better, while the calculations which employed the NLSH bound-nucleon wave function fitted the data from this work better. Further, the data sets demonstrated a slight preference for the EDAD1 optical potential over the EDAI-O optical potential. This was concluded based on the quality of the fits and the more consistent nature of the extracted normalization factors for low  $Q^2$ . As previously mentioned, data set (g) suggested a substantially different normalization.

In the complementary analysis which focused on the 2.442 GeV 1p-shell data obtained in this work, three basic approaches were considered: the fully relativistic approach used in the consistency study [135], the projected approach of Udías et al. [19, 20], and the EMANOSV approach of Kelly [3, 88]. All three approaches included the effects of electron distortion. The fully relativistic approach involved solving the Dirac equation directly in configuration space. The projected approach

TABLE VII: A summary of the kinematic conditions for the  ${}^{16}O(e, e'p)$  consistency study.

|                 |                        |               | $T_p$ | $Q^2$                |             |                             |                       |
|-----------------|------------------------|---------------|-------|----------------------|-------------|-----------------------------|-----------------------|
| label           | authors                | kinematics    | (MeV) | $(\mathrm{GeV}/c)^2$ | x           | $2s_{1/2}1d_{5/2}$ -doublet | data                  |
| a               | Leuschner et al. [13]  | parallel      | 96    | varied               | varied      | resolved                    | reduced $\sigma$      |
| b               | Spaltro et al. [12]    | perpendicular | 84    | 0.20                 | 1.07        | resolved                    | differential $\sigma$ |
| $^{\mathrm{c}}$ | Chinitz et al. [11]    | perpendicular | 160   | 0.30                 | 0.91        | computed $a$                | differential $\sigma$ |
| d               | this work              | perpendicular | 427   | 0.80                 | 0.96        | computed $^{b}$             | differential $\sigma$ |
| e               | Bernheim et al. [10]   | perpendicular | 100   | 0.19                 | 0.90        | computed $^{b}$             | reduced $\sigma$      |
| f               | Blomqvist1 et al. [14] | parallel      | 92    | 0.08                 | 0.30 - 0.50 | resolved                    | reduced $\sigma$      |
| g               | Blomqvist2 et al. [14] | highly varied | 215   | 0.04 - 0.26          | 0.07 - 0.70 | resolved                    | reduced $\sigma$      |

<sup>&</sup>lt;sup>a</sup>The  $1p_{3/2}$ -state data were corrected for the contamination of the doublet by the authors of this work.

TABLE VIII: Normalization factors deduced for the data sets presented in Table VII for  $|P_{\text{miss}}| \leq 200 \text{ MeV}/c$ . The first term in each column is for the  $1p_{1/2}$ -state, while the second term is for the  $1p_{3/2}$ -state.

| _            |               |       |          |      |              |      |          |      |              |      |          |      |              |      |          |      |              |             |          |      |              |      |          |
|--------------|---------------|-------|----------|------|--------------|------|----------|------|--------------|------|----------|------|--------------|------|----------|------|--------------|-------------|----------|------|--------------|------|----------|
|              | EDAI-O        |       |          |      |              |      |          |      |              |      |          |      |              |      |          |      |              | $_{\rm EI}$ | 0AD $1$  |      |              |      |          |
|              |               |       | HS       |      |              | ]    | NLSH     |      |              | NL   | SH-P     |      |              |      | HS       |      |              |             | NLSH     |      |              | NL   | SH-P     |
|              | $S_{\alpha}$  |       | $\chi^2$ |      | $S_{\alpha}$ |      | $\chi^2$ |      | $S_{\alpha}$ |      | $\chi^2$ |      | $S_{\alpha}$ |      | $\chi^2$ |      | $S_{\alpha}$ |             | $\chi^2$ |      | $S_{\alpha}$ |      | $\chi^2$ |
| a            | $0.55 \ 0.46$ | 0.9   | 4.2      | 0.60 | 0.47         | 2.5  | 6.0      | 0.53 | 0.41         | 1.0  | 1.5      | 0.60 | 0.55         | 0.8  | 2.4      | 0.66 | 0.56         | 2.3         | 3.7      | 0.57 | 0.48         | 0.8  | 1.4      |
| b            | $0.61 \ 0.66$ | 2.7   | 6.3      | 0.65 | 0.68         | 5.4  | 8.0      | 0.58 | 0.58         | 2.3  | 3.6      | 0.71 | 0.75         | 2.3  | 5.1      | 0.77 | 0.77         | 4.2         | 6.4      | 0.68 | 0.65         | 2.2  | 4.1      |
| $\mathbf{c}$ | $0.54 \ 0.56$ | 8.7 1 | 7.9      | 0.60 | 0.58         | 24.8 | 25.3     | 0.51 | 0.47         | 9.0  | 15.0     | 0.59 | 0.61         | 8.0  | 18.2     | 0.66 | 0.63         | 16.7        | 22.1     | 0.56 | 0.50         | 7.2  | 23.8     |
| d            | $0.62 \ 0.63$ | 30.8  | 4.7      | 0.70 | 0.65         | 0.5  | 6.7      | 0.59 | 0.52         | 19.6 | 15.3     | 0.62 | 0.63         | 32.5 | 2.4      | 0.70 | 0.66         | 1.2         | 3.9      | 0.60 | 0.53         | 20.0 | 14.4     |
| е            | $0.43 \ 0.46$ | 1.0   | 1.9      | 0.48 | 0.47         | 2.2  | 2.4      | 0.42 | 0.40         | 1.0  | 1.1      | 0.48 | 0.52         | 1.0  | 1.5      | 0.54 | 0.54         | 1.5         | 1.9      | 0.47 | 0.45         | 1.0  | 1.3      |
| f            | $0.53 \ 0.41$ | 3.0   | 4.2      | 0.54 | 0.42         | 5.0  | 5.8      | 0.51 | 0.38         | 2.7  | 1.9      | 0.57 | 0.50         | 3.2  | 3.7      | 0.59 | 0.51         | 5.8         | 5.0      | 0.54 | 0.46         | 2.7  | 2.1      |
| g            | $0.42 \ 0.37$ | 2.0   | 1.4      | 0.44 | 0.37         | 4.7  | 2.0      | 0.40 | 0.33         | 2.5  | 5.9      | 0.42 | 0.40         | 1.8  | 1.9      | 0.44 | 0.41         | 6.6         | 2.8      | 0.40 | 0.36         | 1.9  | 5.4      |

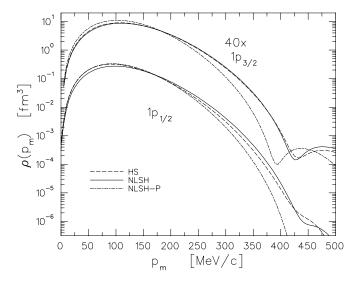


FIG. 11: PWIA momentum distributions for the HS, NLSH, and NLSH-P models. There is only a slight difference between HS and NLSH – for the  $1p_{3/2}$ -state, HS is broader spatially and thus drops off faster with increasing  $P_{\rm miss}$ . On the other hand, NLSH-P differs appreciably from both HS and NLSH, and is clearly distinguishable for  $P_{\rm miss}>250~{\rm MeV}/c$  for both the  $1p_{1/2}$ -state and  $1p_{3/2}$ -state distributions. Note that both the NLSH and NLSH-P wave functions predict binding energies, single-particle energies, and a charge radius for  $^{16}{\rm O}$  which are all in good agreement with the data.

included only the positive-energy components, and as a result, most (but not all) of the spinor distortion was removed from the wave functions. Within the EMA-NOSV approach, a relativized Schrödinger equation was solved using the EMA, and all of the spinor distortion was removed. This made the calculation similar to a factorized calculation, although spin-orbit effects in the initial and final states (which cause small deviations from the factorized results) are included in EMA-NOSV. The current operator was changed between CC1 and CC2. The boundnucleon wave functions HS, NLSH, and NLSH-P were considered. Differences due to the choice of gauge prescription (Coulomb, Weyl, and Landau) were investigated. Because of the large number of optical potentials available at  $T_p \approx 400 \text{ MeV}$ , five were investigated. These potentials included EDAI-O and EDAD1, a slightly modified energy-dependent, atomic-mass dependent parametrization EDAD2 by Cooper et al. [84], as well as MRW by McNeil et al. [108] and RLF by Horowitz [109] and Murdock [110]. Two different nucleon form-factor models (GK by Gari and Krümplemann [111] and the dipole model) were considered. Further, the QMC model of Lu et al. [112, 113] predicts a density dependence for form factors that was calculated and applied to the GK form factors using the Local Density Approximation (see [89]). And finally, the effect of different mixing ratios for the  $2s_{1/2}1d_{5/2}$ -doublet and the  $1p_{3/2}$ -state were considered. The nominal strength of this doublet was taken to be 5% of the strength of the  $1p_{3/2}$ -state using normalization

<sup>&</sup>lt;sup>b</sup>The contamination of the  $1p_{3/2}$ -state doublet was computed by incoherently including the parametrizations of data set (a).

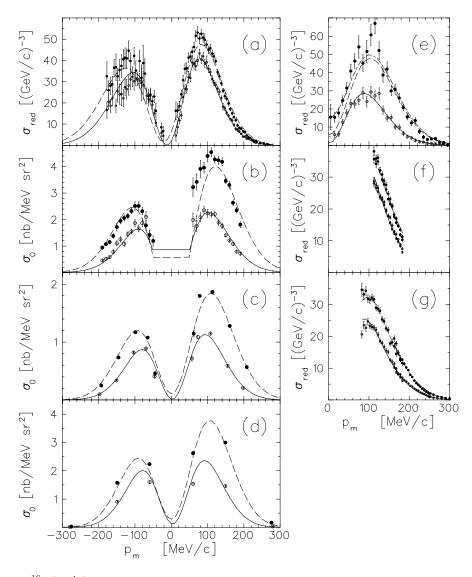


FIG. 12: Fits to various  $^{16}$ O(e,e'p) data sets based on the NLSH bound-nucleon wave function and the EDAI-O optical potential. Open points and solid lines pertain to the  $1p_{1/2}$ -state, while solid points and dashed lines pertain to the  $1p_{3/2}$ -state. The dashed-dotted lines include the contributions of the  $2s_{1/2}1d_{5/2}$ -doublet to the  $1p_{3/2}$ -state. Panel (d) shows the data from this work - see Table VII for the key to the other data sets.

factors determined from data set (a).

Qualitatively, the fully relativistic approach clearly did the best job of reproducing the data. CC2 was in general less sensitive to changes in the bound-nucleon wave function. The choice of wave function primarily affected the  $P_{\rm miss}$ -location of the ripple in  $A_{LT}$  (see Figure 17). Fully relativistic results were shown to be much less gauge-dependent than the nonrelativistic results. The CC2 current operator was also in general less sensitive to choice of gauge, and the data discouraged the choice of the Weyl gauge. The different optical models had little effect on the shape of the calculations, but instead changed the overall magnitude. Both the GK and dipole nucleon form-factor models produced nearly identical results. The change in the calculated GK+QMC cross section was modest, being most pronounced in  $A_{LT}$  for  $P_{\rm miss}$ 

> 300 MeV/c. And finally, the results were best for a 100% contribution of the strength of the  $2s_{1/2}1d_{5/2}$ -doublet to the  $1p_{3/2}$ -state, although the data were not terribly sensitive to this degree-of-freedom.

The basic options employed in the RDWIA calculations presented throughout the rest of this paper (unless otherwise indicated) are summarized in Table X. Note that these options are identical to those used for the calculations first presented in [101].

Figure 13 shows measured cross sections for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  as compared to relativistic calculations at  $E_{\rm beam}=2.442$  GeV. Error bars are statistical, and on average, there is an additional  $\pm 5.6\%$  systematic uncertainty (see Table XII) associated with the data. The solid line is the RDWIA calculation, while the dashed and dashed-dotted

|               | bound-<br>nucleon |       | optical           | nucleon<br>ptical FF           |                |                             |                        |
|---------------|-------------------|-------|-------------------|--------------------------------|----------------|-----------------------------|------------------------|
| prescription  | wavefunction      | gauge | potential         | model                          | (%)            | $\mathrm{S}_{lpha}$         | $\chi^2$               |
| fully EMA-    | NLS               |       | EDA               | GK+                            |                |                             |                        |
| rel proj NOSV | H H-P HS          | C W L | I-O D1 D2 MRW RLF | $\mathrm{GK}\ d\ \mathrm{QMC}$ | $100 \ 50 \ 0$ | CC1 $CC2$                   | CC1 CC2                |
| *             | *                 | *     | *                 | *                              | *              | 0.68 0.62 0.74 0.6          | 7 5.5 5.3 2.0 31.0     |
| *             | *                 | *     | *                 | *                              | *              | 0.78 0.73 0.76 0.7          | 1 17.0 79.0 8.0 70.0   |
| *             | *                 | *     | *                 | *                              | *              | $0.72 \ 0.66 \ 0.75 \ 0.69$ | 9 2.3 65.0 2.2 65.0    |
| *             | *                 | *     | *                 | *                              | *              | 0.60 0.52 0.63 0.54         | 4 10.0 97.0 15.0 115.0 |
| *             | *                 | *     | *                 | *                              | *              | $0.62 \ 0.61 \ 0.65 \ 0.66$ | 5 10.0 6.7 18.0 41.0   |
| *             | *                 | *     | *                 | *                              | *              | 0.63 0.59 0.76 0.76         | 0 25.0 9.2 2.6 22.0    |
| *             | *                 | *     | *                 | *                              | *              | $0.69 \ 0.63 \ 0.73 \ 0.69$ | 7 3.7 6.4 2.5 34.0     |
| *             | *                 | *     | *                 | *                              | *              | 0.64 0.60 0.72 0.6          | 7 29.0 12.0 4.8 8.2    |
| *             | *                 | *     | *                 | *                              | *              | $0.64 \ 0.59 \ 0.71 \ 0.64$ | 5 15.0 6.4 0.7 15.0    |
| *             | *                 | *     | *                 | *                              | *              | $0.62 \ 0.60 \ 0.71 \ 0.6$  | 7 35.0 11.0 7.6 7.3    |
| *             | *                 | *     | *                 | *                              | *              | $0.61 \ 0.58 \ 0.70 \ 0.68$ | 5 41.0 12.0 6.1 7.9    |
| *             | *                 | *     | *                 | *                              | *              | 0.69 0.63 0.75 0.68         | 8 4.8 5.9 2.1 31.0     |
| *             | *                 | *     | *                 | *                              | *              | $0.65 \ 0.61 \ 0.72 \ 0.66$ | 6 11.0 3.3 0.5 16.0    |
| *             | *                 | *     | *                 | *                              | *              | 0.64 0.7                    | 0 6.1 33.0             |
| *             | *                 | *     | *                 | *                              | *              | 0.66 0.73                   | 2 7.4 35.0             |

TABLE IX: Normalization factors derived from the 2.442 GeV 1*p*-shell cross-section data of Table XII using the CC1 and CC2 current operators. The first term in each column is for the  $1p_{1/2}$ -state, while the second term is for the  $1p_{3/2}$ -state.

TABLE X: A summary of the basic options which served as input to the RDWIA calculations presented throughout the rest of this paper (unless otherwise indicated). This input is identical to that used for the calculations first presented in [101].

| Input Parameter           | Option             |
|---------------------------|--------------------|
| bound-state wave function | NLSH               |
| Optical Model             | EDAI-O             |
| nucleon spinor distortion | fully relativistic |
| electron distortion       | yes                |
| current operator          | CC2                |
| nucleon form factors      | GK                 |
| gauge                     | Coulomb            |

lines are respectively the "bare" (no MEC nor IC) ROMEA and RMSGA calculations. The normalization factors for the RDWIA calculations are 0.73 and 0.72 for the  $1p_{1/2}$ -state and  $1p_{3/2}$ -state, respectively. For the ROMEA and RMSGA calculations, they are 0.60 and 0.70, respectively. While the calculations are more-or-less indistinguishable for  $|P_{\rm miss}| < 125~{\rm MeV}/c$ , the RDWIA calculations do a far better job of representing the data over the entire  $P_{\rm miss}$  range.

Suggested to delete this text and the corresponding figure as redundant: Figure 14 shows measured cross sections for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  as compared to relativistic calculations at  $E_{\rm beam}=2.442$  GeV plotted on a linear scale. As before, error bars are statistical, and on average, there is an additional  $\pm 5.6\%$  systematic uncertainty (see Table XII) associated with the data. The top panel is again the RDWIA calculation, while the middle and bottom panels are respectively the "bare" (no MEC nor IC) ROMEA and RMSGA calculations. As previously mentioned, there is little to distinguish between

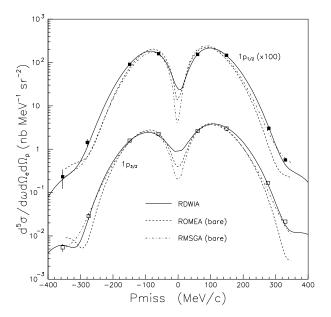


FIG. 13: Measured cross sections for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  as compared to relativistic calculations at  $E_{\rm beam}=2.442~{\rm GeV}.$  Error bars are statistical, and on average, there is an additional  $\pm 5.6\%$  systematic uncertainty (see Table XII) associated with the data. The solid line is the RDWIA calculation, while the dashed and dashed-dotted lines are respectively the "bare" (no MEC nor IC) ROMEA and RMSGA calculations.

the calculations for  $|P_{\rm miss}| < 125~{\rm MeV}/c$ , but the RDWIA calculations do a far better job of representing the data over the entire  $P_{\rm miss}$  range.

Figure 15 shows the left-right asymmetry  $A_{LT}$  together

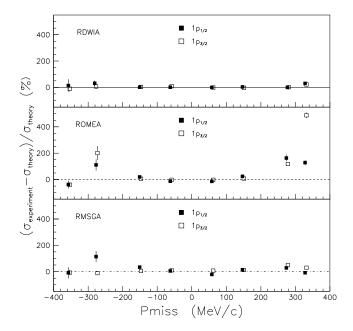


FIG. 14: Suggested to delete this figure as redundant: Measured cross sections for the removal of protons from the 1p-shell of  $^{16}\mathrm{O}$  as a function of  $P_{\mathrm{miss}}$  as compared to relativistic calculations at  $E_{\mathrm{beam}}=2.442~\mathrm{GeV}$ . Error bars are statistical, and on average, there is an additional  $\pm 5.6\%$  systematic uncertainty (see Table XII) associated with the data. The top panel is the RDWIA calculation, while the middle and bottom panels are respectively the "bare" (no MEC nor IC) ROMEA and RMSGA calculations.

with relativistic calculations for the removal of protons from the 1p-shell of  $^{16}$ O as a function of  $P_{\text{miss}}$  for  $E_{\text{beam}} =$ 2.442 GeV. Error bars are statistical (see Table XXV for the associated systematic uncertainties). The solid line is the RDWIA calculation, while the dashed and dasheddotted lines are respectively the "bare" (no MEC nor IC) ROMEA and RMSGA calculations. Note that the EA calculations stop at  $P_{\rm miss}=350~{\rm MeV}/c$  as the approximation becomes invalid. Note also the large change in the slope of  $A_{LT}$  at  $P_{\text{miss}} \approx 300 \text{ MeV}/c$ . While all three calculations undergo a similar change in slope, it is the RDWIA calculation which does the best job of reproducing it. The ROMEA calculation reproduces the data well for  $P_{\rm miss} < 300 \ {\rm MeV}/c$ , but substantially overestimates  $A_{LT}$ for  $P_{\rm miss} > 300~{\rm MeV}/c$ . The RMSGA calculation does well with the overall trend in the data, but struggles with the overall normalization for knockout from the  $1p_{1/2}$ -state.

Figure 16 shows the left-right asymmetry  $A_{LT}$  together with RDWIA calculations for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442~{\rm GeV}$ . Error bars are statistical (see Table XXV for the associated systematic uncertainties). In this figure, the nature of the large change in the slope of  $A_{LT}$  at  $P_{\rm miss}\approx 300~{\rm MeV}/c$  is addressed. The solid curves are

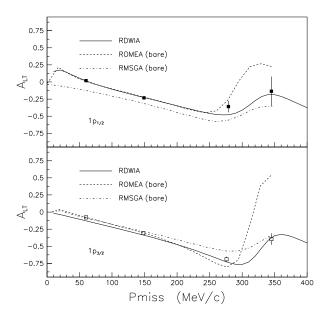


FIG. 15: Left-right asymmetry  $A_{LT}$  together with relativistic calculations of the  $A_{LT}$  asymmetry for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442~{\rm GeV}$ . Error bars are statistical (see Table XXV for the associated systematic uncertainties). The solid line is the RD-WIA calculation, while the dashed and dashed-dotted lines are respectively the "bare" (no MEC nor IC) ROMEA and RMSGA calculations.

the RDWIA calculations identical to those shown in Figure 15. The effect is due to the distortion of the boundnucleon and ejectile spinors, as evidenced by the other three curves shown, in which the full RDWIA calculation has been "decomposed". It is important to note, however, that these three curves all retain the same basic ingredients, particularly the fully relativistic current operator and the upper components of the Dirac spinors. Of the three curves, the dotted line resulted from a calculation where only the bound-nucleon spinor distortion was included, the dashed line resulted from a calculation where only the scattered-state spinor distortion was included, and the dashed-dotted line resulted from a calculation where undistorted spinors (essentially identical to a factorized calculation) were considered. Clearly, the inclusion of the bound-nucleon spinor distortion is more important than the inclusion of the scattered-state spinor distortion, but both are necessary to describe the data.

Figure 17 shows the  $P_{\rm miss}$ -dependence of the left-right asymmetry  $A_{LT}$  for the  $1p_{1/2}$ -state for  $E_{\rm beam}=2.442$  GeV together with RDWIA calculations. Error bars are statistical (see Table XXV for the associated systematic uncertainties). The solid curves in all three panels are the same and are identical to those shown for the removal of protons from the  $1p_{1/2}$ -state of  $^{16}{\rm O}$  in Figures 15 and 16. In the top panel, the EDAI-O optical potential and NLSH bound-nucleon wave function were used for all the cal-

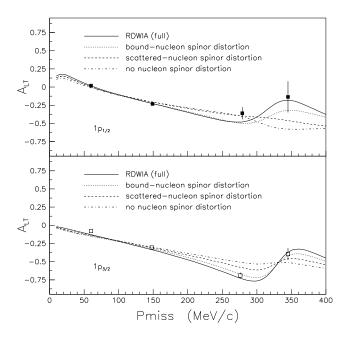


FIG. 16: Left-right asymmetry  $A_{LT}$  together with RDWIA calculations for the removal of protons from the 1*p*-shell of <sup>16</sup>O as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Error bars are statistical (see Table XXV for the associated systematic uncertainties). Note that the solid curves shown in this figure are identical to those shown in Figure 15.

culations, but the choice of current operator was varied between CC1 (dashed), CC2 (solid), and CC3 (dasheddotted), resulting in a change in both the height and the  $P_{\text{miss}}$ -location of the ripple in  $A_{LT}$ . In the middle panel, the current operator CC2 and EDAI-O optical potential were used for all the calculations, but the choice of bound-nucleon wave function was varied between NLSH-P (dashed), NLSH (solid), and HS (dashed-dotted), resulting in a change in the  $P_{\rm miss}$ -location of the ripple, but a relatively constant height. In the bottom panel, the current operator CC2 and NLSH bound-nucleon wave function were used for all the calculations, but the choice of optical potential was varied between EDAD1 (dashed), EDAI-O (solid), and EDAD2 (dashed-dotted), resulting in a change in the height of the ripple, but a relatively constant  $P_{\rm miss}\text{-location}.$  More high-precision data, particularly for  $150 < P_{\text{miss}} < 400 \text{ MeV}/c$  are clearly needed to accurately determine the current operator, the boundstate wave function, the optical potential, and of course the normalization factors simultaneously. This experiment has recently been performed in Hall A at Jefferson Lab by Saha et al. [114], and the results are currently under analysis.

Figure 18 shows the  $R_{L+TT}$ ,  $R_{LT}$ , and  $R_T$  effective response functions together with relativistic calculations for the removal of protons from the 1p-shell of  $^{16}\mathrm{O}$  as a function of  $P_{\mathrm{miss}}$ . The effective response functions are

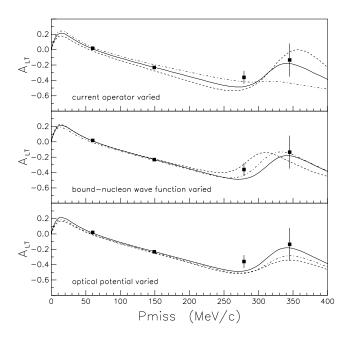


FIG. 17: Left-right asymmetry  $A_{LT}$  together with RDWIA calculations for the removal of protons from the  $1p_{1/2}$ -state of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Error bars are statistical (see Table XXV for the associated systematic uncertainties). The solid curves in all three panels are the same and are identical to those shown for the removal of protons from the  $1p_{1/2}$ -state of  $^{16}{\rm O}$  in Figures 15 and 16.

theoretically determined by calculating cross sections at the experimental kinematics and then analyzing these calculated cross sections using the one-photon exchange framework of Equation (4). Error bars are statistical. Note that the data point located at  $P_{\rm miss} \approx 52 \ {\rm MeV}/c$ comes from the parallel kinematics measurements [136] (see Table XXIII), while the other data points come from the perpendicular kinematics measurements (see Tables XXV and XXIV). The systematic uncertainties associated with these data points are also presented in the aforementioned Tables. The solid line is the RDWIA calculation, while the dashed and dashed-dotted lines are respectively the "bare" (no MEC nor IC) ROMEA and RMSGA calculations. Note that the EA calculations stop at  $P_{\rm miss} = 350 \ {\rm MeV}/c$  as the approximation becomes invalid. The agreement, particularly between the RDWIA and ROMEA calculations and the data is very good. The spinor distortions in the RDWIA calculations which were required to predict the change in slope of  $A_{LT}$  at  $P_{\text{miss}} \approx$ 300 MeV/c in Figure 16 are also essential to the description of  $R_{LT}$ . The agreement between the RMSGA calculations and the data, particularly for  $R_{LT}$ , is markedly

Qualitatively, it should be noted that none of the calculations presented so far include contributions from twobody currents. The good agreement between the cal-

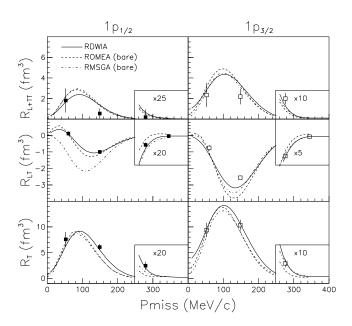


FIG. 18: Data from this work together with relativistic calculations for the  $R_{L+TT}$ ,  $R_{LT}$ , and  $R_T$  response functions for the removal of protons from the 1p-shell of <sup>16</sup>O as a function of  $P_{\rm miss}$ . Error bars are statistical (see Tables XXIV, XXV, and XXIII for the associated systematic uncertainties). The solid line is the RDWIA calculation, while the dashed and dashed-dotted lines are respectively the "bare" ROMEA and RMSGA calculations.

culations and the data indicates that these currents are already small at  $Q^2=0.8~({\rm GeV}/c)^2$ . This observation is supported by independent calculations by Amaro et~al.~[115,116] which estimate the importance of such currents (which are highly dependent on  $P_{\rm miss}$ ) to be large at lower  $Q^2$ , but only 2% for the  $1p_{1/2}$ -state and 8% for the  $1p_{3/2}$ -state in these kinematics. It should also be noted that these RDWIA results are comparable with those obtained in independent RDWIA analyses of our data by the Pavia Group (see Meucci et~al.~[117]).

## 2. Two-body current contributions

In this section, two-body current contributions to the ROMEA and RMSGA calculations stemming from MEC and IC are presented. Said contributions to the transition matrix elements were determined within the non-relativistic framework outlined by Ryckebusch *et al.* in [118, 119].

Figure 19 shows measured cross sections for the removal of protons from the 1p-shell of  $^{16}\mathrm{O}$  as a function of  $P_{\mathrm{miss}}$  as compared to calculations by the Ghent Group which include MEC and IC at  $E_{\mathrm{beam}}=2.442~\mathrm{GeV}$ . Error bars are statistical, and on average, there is an additional

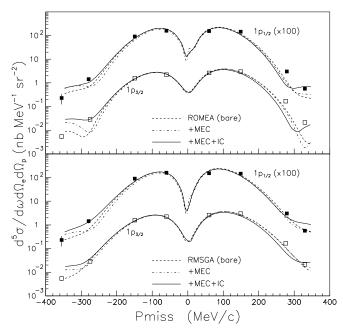


FIG. 19: Measured cross sections for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  together with calculations by the Ghent Group at  $E_{\rm beam}=2.442$  GeV. Error bars are statistical, and on average, there is an additional  $\pm 5.6\%$  systematic uncertainty (see Table XII). The curves labelled "bare" are identical to those shown in Figure 13.

 $\pm 5.6\%$  systematic uncertainty (see Table XII) associated with the data. In the top panel, ROMEA calculations are shown. The dashed line is the "bare" (no MEC nor IC) calculation, the dashed-dotted line includes MEC, and the solid line includes both MEC and IC. In the bottom panel, RMSGA calculations are shown. The dashed line is the "bare" (no MEC nor IC) calculation, the dasheddotted line includes MEC, and the solid line includes both MEC and IC. Note that the curves labelled "bare" are identical to those shown in Figure 13. The normalization factors are 0.60 and 0.70 for the  $1p_{1/2}$ -state and  $1p_{3/2}$ state, respectively. The impact of the two-body currents on the computed differential cross sections for the knockout of 1p-shell from  $^{16}{\rm O}$  is no more than a few percent for low  $P_{\text{miss}}$ , but gradually increases with increasing  $P_{\text{miss}}$ . Surprisingly, explicit inclusion of the two-body current contributions to the transition matrix elements does not markedly improve the overall agreement between the calculations and the data.

Figure 20 shows the left-right asymmetry  $A_{LT}$  together with calculations by the Ghent Group for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Error bars are statistical (see Table XXV for the associated systematic uncertainties). In the top two panels, ROMEA calculations are shown. The dashed line is the "bare" (no MEC nor IC) calculation, the dashed-dotted line includes MEC, and the solid line includes both MEC and IC. In the bottom panel, RMSGA calculations are shown. The dashed line is the "bare"

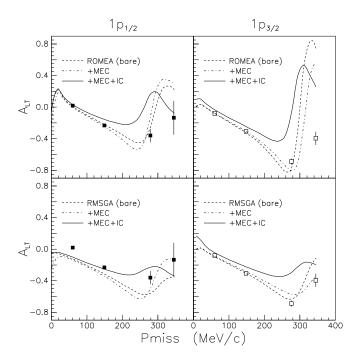


FIG. 20: Left-right asymmetry  $A_{LT}$  together with calculations by the Ghent Group of the  $A_{LT}$  asymmetry for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$  for  $E_{\rm beam}=2.442$  GeV. Error bars are statistical (see Table XXV for the associated systematic uncertainties). The curves labelled "bare" are identical to those shown in Figure 15.

(no MEC nor IC) calculation, the dashed-dotted line includes MEC, and the solid line includes both MEC and IC. Again, the calculations stop at  $P_{\rm miss}=350~{\rm MeV}/c$  as the EA becomes invalid. While all three calculations undergo a change in slope at  $P_{\rm miss}=300~{\rm MeV}/c$ , it is again clearly the "bare" calculations which best represent the data. Note that in general, the IC were observed to produce larger effects than the MEC.

Figures 21 and 22 show the  $R_{L+TT}$ ,  $R_{LT}$ , and  $R_T$  response functions together with ROMEA and RMSGA calculations (respectively) by the Ghent Group for the removal of protons from the 1*p*-shell of  $^{16}$ O as a function of  $P_{\text{miss}}$ . Error bars are statistical. The systematic uncertainties associated with these data points are presented in Tables XXIII, XXV, and XXIV. The dashed lines are the "bare" (no MEC nor IC) ROMEA and RMSGA calculations, while the solid lines include both MEC and IC. Again, the calculations stop at  $P_{\text{miss}} = 350 \text{ MeV}/c$  as the EA becomes invalid. In contrast to the cross section (recall Figure 19) and  $A_{LT}$  (recall Figure 20) situations, the agreement between the response-function data and the calculations improves dramatically with the explicit inclusion of the two-body current contributions to the transition matrix elements.

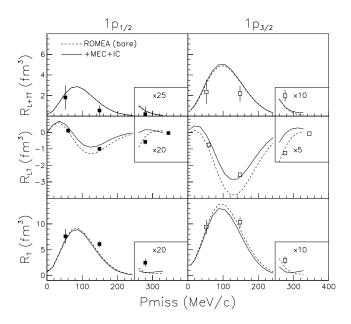


FIG. 21: Data from this work together with ROMEA calculations by the Ghent Group for the  $R_{L+TT}$ ,  $R_{LT}$ , and  $R_T$  response functions for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$ . Error bars are statistical (see Tables XXIV, XXV, and XXIII for the associated systematic uncertainties). The curves labelled "bare" are identical to those shown in Figure 18.

## B. Higher missing energies

Figure 23 presents averaged measured cross sections as a function of  $E_{\text{miss}}$  obtained at  $E_{\text{beam}} = 2.442 \text{ GeV}$  for four discrete  $HRS_h$  angular settings ranging from  $2.5^{\circ}$  <  $\theta_{pq} < 20^{\circ}$ , corresponding to average values of  $P_{\rm miss}$  increasing from 50 MeV/c to 340 MeV/c. The cross-section values shown are the averaged values of the cross sections measured on either side of  $\vec{q}$  at each  $\theta_{pq}$ . The strong peaks at  $E_{\rm miss}=12.1$  and 18.3 MeV correspond to 1p-shell proton removal from <sup>16</sup>O. As in Section V A, the dashed curves corresponding to these peaks are the "bare" (no MEC nor IC) ROMEA calculations, while the solid lines include both MEC and IC. The normalization factors remain 0.70 and 0.60 for the  $1p_{1/2}$ - and  $1p_{3/2}$ -states, respectively. For  $E_{\rm miss} > 20$  MeV, the spectra behave in a completely different fashion. appreciable strength exists which scales roughly with the 1p-shell fragments and is not addressed by the present calculations of two-nucleon knockout. This strength has been studied in  $(\gamma, p)$  experiments, and has been interpreted by the Ghent Group [120] as the post-photoabsorption population of states with a predominant 2h1p character via two-body currents. For  $E_{\rm miss} > 30$  MeV, in the top panel for  $P_{\rm miss} \approx$ 50 MeV/c, there is a broad and prominent peak centered

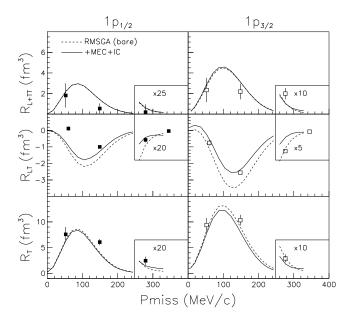


FIG. 22: Data from this work together with RMSGA calculations by the Ghent Group for the  $R_{L+TT}$ ,  $R_{LT}$ , and  $R_T$  response functions for the removal of protons from the 1p-shell of  $^{16}{\rm O}$  as a function of  $P_{\rm miss}$ . Error bars are statistical (see Tables XXIV, XXV, and XXIII for the associated systematic uncertainties). The curves labelled "bare" are identical to those shown in Figure 18.

at  $E_{\rm miss} \approx 40 \, {\rm MeV}$  corresponding largely to the knockout of  $1s_{1/2}$ -state protons. As can be seen in the lower panels, the strength of this peak diminishes with increasing  $P_{\rm miss}$ , and completely vanishes beneath a flat background by  $P_{\rm miss} \approx 280~{\rm MeV}/c$ . For  $E_{\rm miss} > 60~{\rm MeV}$  and  $P_{\rm miss} >$  $280~{
m MeV}/c$ , the cross section decreases only very weakly as a function of  $P_{\text{miss}}$ , and is completely independent of  $E_{\rm miss}$ . In order to estimate how much of the cross section observed for  $E_{\rm miss} > 25$  MeV can be explained by the single-particle knockout of protons from the  $1s_{1/2}$ -state, the data were also compared to the ROMEA calculations of the Ghent Group. The dashed curves are the "bare" (no MEC nor IC) ROMEA calculations, while the solid lines include both MEC and IC. A normalization factor of 1.00 with respect to the single-particle strength for the  $1s_{1/2}$ -state was chosen. The two calculations are indistinguishable for  $P_{\rm miss} < 145~{\rm MeV}/c$ . The agreement between calculations and the measured cross sections (see the top two panels of Figure 23) for  $P_{\rm miss} \leq 145~{\rm MeV}/c$ (where there is an identifiable  $1s_{1/2}$ -state peak at  $E_{\rm miss}$  $\approx 40 \text{ MeV}$ ) is reasonable. At higher  $P_{\text{miss}}$  (where there is no clear  $1s_{1/2}$ -state peak at  $E_{\rm miss} \approx 40 \, {\rm MeV}$ ) the data are substantially larger than the calculated "bare" cross section. Inclusion of MEC and IC improve the agreement, but there is still roughly an order-of-magnitude discrepancy. The RDWIA calculations demonstrate similar behavior. Thus, the  $P_{\rm miss} \geq 280 \ {\rm MeV}/c$  data is not dominated by single-particle knockout. Note that the magnitude of  $(S_T - S_L)$  is consistent with that anticipated based on the measurements of Ulmer et al. at  $Q^2 = 0.14$  $(\text{GeV}/c)^2$  and Dutta et al. at  $Q^2 = 0.6$  and 1.8  $(\text{GeV}/c)^2$ . Together, these data suggest that transverse processes associated with the knockout of more than one nucleon decrease with increasing  $Q^2$ . Also shown as dashed-dotted curves in Figure 23 are the calculations of the by Janssen et al. [121] for the (e, e'pp) and (e, e'pn) contributions to the (e, e'p) cross section performed within a Hartree-Fock framework. These two-particle knockout cross sections were determined using the spectator approximation, in a calculation which included pion-exchange currents, the creation of an intermediate  $\Delta(1232)$ , and both central and tensor short-range correlations. In these kinematics, the two-body pion-exchange and  $\Delta(1232)$  currents account for roughly 85% of the calculated two-particle knockout strength, short-range tensor correlations account for about 13%, and short-range central correlations account for approximately 2\%. The calculated twoparticle knockout cross sections are essentially transverse in nature, since the two-body currents are predominantly transverse. The calculated strength underestimates the measured cross section by about 50% but has the observed flat shape for  $E_{\rm miss} > 50$  MeV. It is thus possible that heavier meson exchange and processes involving three (or more) nucleons could provide a complete description of the data.

The separated response functions  $R_{L+TT}$ ,  $R_{LT}$ , and  $R_T$  together with ROMEA calculations for  $P_{\rm miss}=145$  ${\rm MeV}/c$  and  $P_{\rm miss}$  = 280  ${\rm MeV}/c$  are presented in Figure 24. Kinematic overlap restricted separations to  $E_{\rm miss}$ < 60 MeV. The error bars are statistical (see Tables XXVII and XXVIII for the associated systematic uncertainties). The dashed curves are the "bare" (no MEC nor IC) ROMEA calculations, while the solid curves include both MEC and IC. Also shown as dashed-dotted curves are the incoherent sum of these "full" calculations and the computed (e, e'pp) and (e, e'pn) contribution. In general, the response functions do not demonstrate the broad peak centered at  $E_{\rm miss} \approx 40$  MeV corresponding to the knockout of  $1s_{1/2}$ -state protons and predicted by the calculations. At  $P_{\text{miss}} = 145 \text{ MeV}/c$ , the "bare" calculation is consistently about 60% of the data. Inclusion of MEC and IC does not appreciably affect the magnitude of  $R_{L+TT}$ , but does improve the agreement between data and calculation for  $R_{LT}$  and  $R_{T}$ .  $R_{L+TT}$  (which is essentially equal to  $R_{L}$  since  $\frac{v_{TT}}{v_{L}}R_{TT}$  is roughly 7% of  $R_L$  in these kinematics) is about 50% of the data. The agreement between the calculation and the data for  $R_{LT}$  is very good over the entire  $E_{\text{miss}}$  range. Since  $R_{LT}$  is nonzero for  $E_{\text{miss}} > 50$  MeV,  $R_L$  must also be nonzero.  $R_T$  is somewhat larger than the calculation for  $E_{\rm miss} < 60$  MeV. At  $P_{\rm miss} = 280$  MeV/c, the "bare" calculation does not reproduce the  $E_{\text{miss}}$ -dependence of any of the response functions. The inclusion of MEC and IC in the calculation substantially increases the magni-

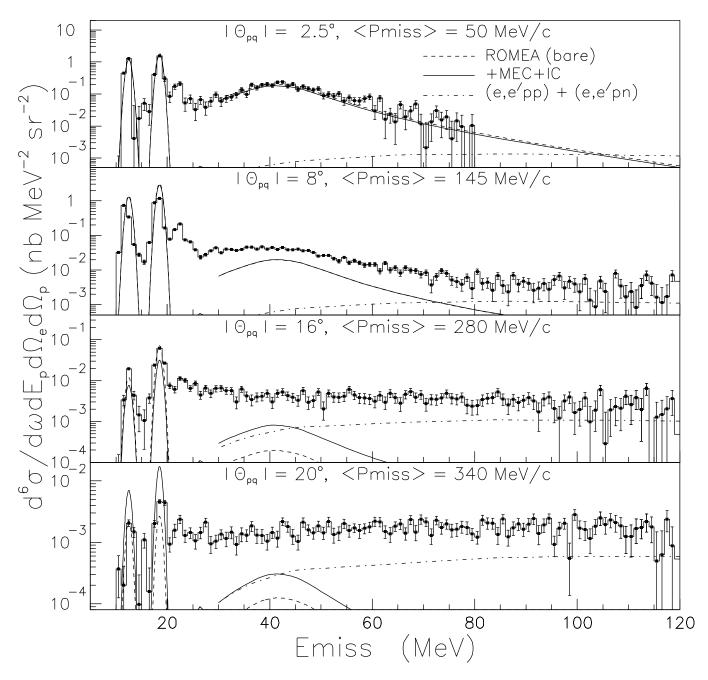


FIG. 23: Data from this work together with ROMEA calculations by the Ghent Group for the  $E_{\text{miss}}$ -dependence of the cross sections obtained at  $E_{\text{beam}} = 2.442$  GeV. The data are the average cross sections measured on either side of  $\vec{q}$  at each  $\theta_{pq}$ . Error bars are statistical and on average, there is an additional  $\pm 5.9\%$  systematic uncertainty (see Tables XVIII – XXII) associated with the data. Also shown are calculations by the Ghent Group for the (e, e'pp) and (e, e'pn) contributions to the (e, e'p) cross section.

tude of all three calculated response functions, and thus improves the agreement between data and calculation.  $R_{L+TT}$  (dominated by  $R_L$  [89]) is consistent with both the calculation and with zero.  $R_{LT}$  is about twice the magnitude of the calculation. Since  $R_{LT}$  is nonzero over the entire  $E_{\rm miss}$  range,  $R_L$  must also be nonzero.  $R_T$  is significantly larger than both the calculation and zero out to at least  $E_{\rm miss}=60$  MeV. The fact that  $R_T$  is much larger than  $R_L$  indicates the cross section is largely due

to transverse two-body currents. And finally, it is clear that (e,e'pX) accounts for a fraction of the measured transverse strength which increases dramatically with increasing  $P_{\rm miss}$ .

Figure 25 shows the calculations by the Ghent Group [99] of the contribution to the differential  $^{16}\text{O}(e,e'p)$  cross section from two-nucleon knockout as a function of  $E_{\text{miss}}$  and  $\theta_p$  for  $E_{\text{beam}}=2.442$  GeV. The upper-left panel shows the contribution of central correlations.

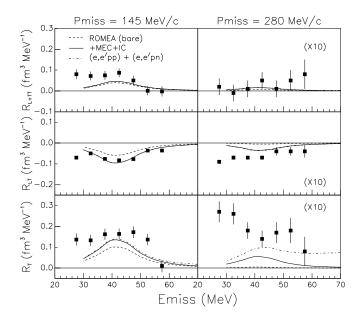


FIG. 24: Data from this work together with ROMEA calculations by the Ghent Group for the  $E_{\rm miss}$ -dependence of the  $R_{L+TT},\,R_{LT},\,$  and  $R_T$  response functions. Error bars are statistical (see Tables XXVII, XXVIII, and XXVI for the associated systematic uncertainties). Also shown is the (e,e'pX) contribution.

The upper-right panel shows the combined contribution of central and tensor correlations. Tensor correlations are anticipated to dominate central correlations over the ranges of  $E_{\rm miss}$  and  $P_{\rm miss}$  investigated in this work. The lower-left panel shows the combined contribution of central and tensor correlations (two-nucleon correlations) together with MEC and IC (two-body currents). Two-body currents are anticipated to dominate two-nucleon correlations over the ranges of  $E_{\rm miss}$  and  $P_{\rm miss}$  investigated in this work. For convenience, the variation of  $P_{\rm miss}$  with  $E_{\rm miss}$  and  $\theta_p$  is shown in the bottom-right panel.

## VI. SUMMARY AND CONCLUSIONS

The  $^{16}{\rm O}(e,e'p)$  reaction in QE, constant  $(q,\omega)$  kinematics at  $Q^2\approx 0.8~({\rm GeV}/c)^2,~|\vec{q}|\approx 1~{\rm GeV}/c,$  and  $\omega\approx 439~{\rm MeV}$  was measured for  $0< E_{\rm miss}< 120~{\rm MeV}$  and  $0< P_{\rm miss}< 350~{\rm MeV}/c.$  Five-fold differential cross sections for the removal of protons from the 1p-shell were obtained for  $0< P_{\rm miss}< 350~{\rm MeV}/c.$  Six-fold differential cross sections for  $0< E_{\rm miss}< 120~{\rm MeV}$  were obtained for  $0< P_{\rm miss}< 350~{\rm MeV}/c.$  These results were used to extract the  $A_{LT}$  asymmetry and the  $R_L$ ,  $R_T$ ,  $R_{L+TT}$ , and  $R_{LT}$  response functions over a large range of  $E_{\rm miss}$  and  $P_{\rm miss}$ .

The data were interpreted in subsets corresponding to the 1p-shell and the  $1s_{1/2}$ -state and continuum, respectively. 1p-shell data were interpreted within three fully relativistic frameworks for single-particle knockout which do not include any two-body currents: RDWIA,

ROMEA, and RMSGA. Two-body current contributions to the ROMEA and RMSGA calculations for the 1p-shell stemming from MEC and IC were then also considered. The  $1s_{1/2}$ -state and continuum data were considered within the identical ROMEA framework before two-body current contributions due MEC and IC were included. (e, e'pX) contributions to these data were also examined.

Overall, the RDWIA calculations provided by far the best description of the 1p-shell data. Dynamic effects due to the inclusion of the lower components of the Dirac spinors in RDWIA calculations were necessary to self-consistently reproduce the 1p-shell cross sections, the  $A_{LT}$  asymmetry, and the  $R_{LT}$  response function over the entire measured range of  $P_{\text{miss}}$ . Within the RD-WIA framework, the four most important ingredients were the inclusion of both bound-nucleon and ejectile spinor distortion, the choice of current operator, the choice of bound-nucleon wave function, and the choice of optical potential. Inclusion of the spinor distortion resulted in a diffractive "wiggle" in  $A_{LT}$  at  $P_{\text{miss}} = 325 \text{ MeV}/c$  which agreed nicely with the data. A different choice of current operator either damped out or magnified this "wiggle". A different choice of bound-nucleon wave function changed the  $P_{\text{miss}}$ -location of the "wiggle", but preserved the magnitude. A different choice of optical potential changed the magnitude of the "wiggle" but preserved the  $P_{\text{miss}}$ location.

As anticipated, since  $p_p \approx 1~{\rm GeV}/c$ , the ROMEA calculations provided a reasonable description of the 1p-shell data. For this energy range, optical models generally provide an overall better description of proton elastic scattering than does the Glauber model. This is in part due to important medium modifications of the NN interaction from Pauli blocking and spinor distortion. Surprisingly, the unfactorized "out-of-the-box" RMSGA calculations provided a fairly good description of the 1p-shell data already at this relatively low proton momentum. Adding the contributions of two-body currents due to MEC and IC to the descriptions of the 1p-shell data provided by the "bare" ROMEA and RMSGA calculations did not improve the agreement.

For  $25 < E_{\text{miss}} < 50 \text{ MeV}$  and  $P_{\text{miss}} < 145 \text{ MeV}/c$ , the reaction was dominated by the knockout of  $1s_{1/2}$ state protons and the cross sections and response functions were reasonably well-described by "bare" ROMEA calculations which did not consider the contributions of two-body currents due to MEC and IC. However, as  $P_{\text{miss}}$ increased beyond 145 MeV/c, the single-particle aspect of the reaction diminished. Cross sections and response functions were no longer "peaked" at  $E_{\text{miss}} = 40 \text{ MeV}$ , nor did they exhibit the Lorenzian s-shell shape. Already at  $P_{\rm miss}=280~{\rm MeV}/c$ , the same "bare" ROMEA calculations that did well describing the data for  $P_{\rm miss}$  < 145 MeV/c underestimated the cross section data by more than a decade. Including the contributions of two-body currents due to MEC and IC improved the agreement for  $E_{\rm miss} < 50$  MeV, but the calculations still dramatically underpredict the data.

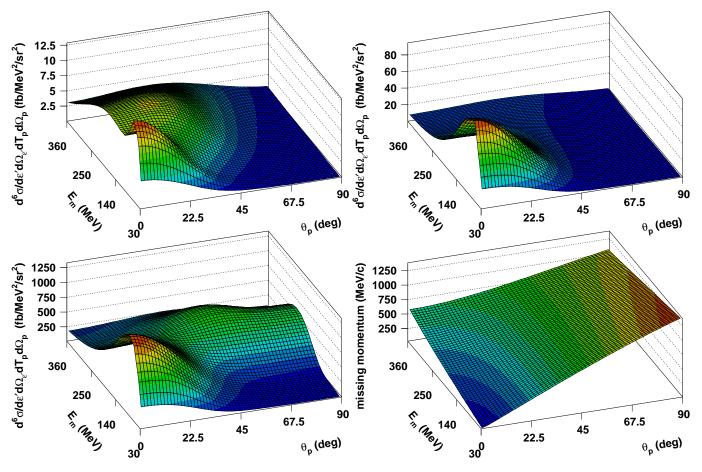


FIG. 25: Calculations by the Ghent Group [99] of the contribution to the differential  $^{16}\text{O}(e,e'p)$  cross section from two-nucleon knockout as a function of  $E_{\text{miss}}$  and  $\theta_p$  for  $E_{\text{beam}} = 2.442$  GeV. The upper-left panel shows the contribution of central correlations. The upper-right panel shows the combined contribution of central and tensor correlations. The lower-left panel shows the combined contribution of central and tensor correlations (two-nucleon correlations) together with MEC and IC (two-body currents). The relationship between the various kinematic quantities is shown in the bottom-right panel.

For  $25 < E_{\rm miss} < 120$  MeV and  $P_{\rm miss} \ge 280$  MeV/c, the cross section was almost constant as a function of both  $P_{\rm miss}$  and  $E_{\rm miss}$ . Here, the single-particle aspect of the  $1s_{1/2}$ -state contributed < 10% to the cross section. Two-nucleon (e,e'pX) calculations accounted for only about 50% of the magnitude of the cross section data, but reproduced the shape well. Also, they predicted the magnitude of  $R_T$  for  $E_{\rm miss} > 60$  MeV. The model, which explained the shape, transverse nature, and 50% of the measured cross section, suggested that the contributions of the two-nucleon current due to MEC and IC are much larger than those of the two-nucleon correlations. The measured cross section that remains unaccounted for suggests additional currents and processes play an equally important role.

## Acknowledgments

We acknowledge the outstanding support of the staff of the Accelerator and Physics Divisions at Jefferson Laboratory that made this experiment successful. We thank T. W. Donnelly and J. W. Van Orden for valuable discussions. This work was supported in part by the U. S. Department of Energy contract DE-AC05-84ER40150 under which the Southeastern Universities Research Association (SURA) operates the Thomas Jefferson National Accelerator Facility, other Department of Energy contracts, the National Science Foundation, the Swedish Research Council, the Italian Istituto Nazionale di Fisica Nucleare (INFN), the French Atomic Energy Commission and National Center of Scientific Research, and the Natural Sciences and Engineering Research Council of Canada.

## APPENDIX A: QUASIELASTIC RESULTS

#### 1. Cross sections

## a. 1p-shell

Cross sections for QE proton knockout from the 1p-shell of <sup>16</sup>O are presented in Tables XI and XII.

TABLE XI: Measured cross sections for QE proton knockout from the 1p-shell of  $^{16}{\rm O}$  for  $< T_p > = 427$  MeV. The  $P_{\rm miss}$  bins were 20 MeV/c wide. Cuts were applied to remove the radiative tail from  $^{1}{\rm H}(e,ep)$  such that  $< P_{\rm miss} > = 52.5$  MeV/c in each case. While the HRS\_h was aligned along  $\vec{q}$ , this data set does not truly correspond to parallel kinematics because of these cuts. Since  $\vec{p}_p$  and  $\vec{q}$  had about the same magnitude,  $\vec{P}_{\rm miss}$  arose from the slight angles between them, not from differences in their magnitudes. However, since the distribution of  $\vec{P}_{\rm miss}$  was symmetrical about  $\vec{q}$ , the conditions of parallel kinematics are closely approximated.

|                                 |                      |            | $1p_{1/2}$ -                            |                   |                    |       |   |     |  |
|---------------------------------|----------------------|------------|---|-------------------|--------------------|-------|---|-----|--|
| $E_{\mathrm{beam}} \theta_{pq}$ | $< Q^2 >$            | $<\omega>$ | $d^5\sigma/d\omega d\Omega_e d\Omega_p$ | $\delta^{ m sys}$ | $< Q^2 >$          |       | $d^5\sigma/d\omega d\Omega_e d\Omega_p$ |     |  |
| (GeV) (°)                       | $(\mathrm{GeV}/c)^2$ | (MeV)      | $(nb/MeV \cdot sr^2)$                   | (%)               | $(\text{GeV}/c)^2$ | (MeV) | $(nb/MeV \cdot sr^2)$                   | (%) |  |
| 0.843 0.0                       | 0.810                | 436.0      | $0.0922 \pm 0.0118$                     | 5.4               | 0.810              | 436.0 | $0.1143 \pm 0.0115$                     | 5.4 |  |
| 1.643 0.0                       | 0.820                | 421.5      | $0.5827 \pm 0.0486$                     | 5.5               | 0.820              | 421.5 | $0.7418 \pm 0.0514$                     | 5.4 |  |
| 2.442 0.0                       | 0.815                | 423.0      | $1.5030 \pm 0.1380$                     | 5.5               | 0.815              | 423.0 | $1.8540 \pm 0.1500$                     | 5.5 |  |

TABLE XII: Measured cross sections for QE proton knockout from the 1p-shell of  $^{16}{\rm O}$  for  $< Q^2>=0.800~({\rm GeV}/c)^2, < \omega>=436~{\rm MeV},$  and  $< T_p>=427~{\rm MeV}.$  The  $P_{\rm miss}$  bins were 20 MeV/c wide.

| <u> </u>            |               |                    | $1p_{1/2}$ -:                           | state             |                    | 1p <sub>3/2</sub> -s                    | state             |
|---------------------|---------------|--------------------|---|-------------------|--------------------|---|-------------------|
| $E_{\mathrm{beam}}$ | $\theta_{pq}$ | $< P_{\rm miss} >$ | $d^5\sigma/d\omega d\Omega_e d\Omega_p$ | $\delta^{ m sys}$ | $< P_{\rm miss} >$ | $d^5\sigma/d\omega d\Omega_e d\Omega_p$ | $\delta^{ m sys}$ |
| (GeV)               | (°)           | (MeV/c)            | $(nb/MeV \cdot sr^2)$                   | (%)               | (MeV/c)            | $(nb/MeV \cdot sr^2)$                   | (%)               |
| 0.843               | 8.0           | 150.0              | $0.0789 \pm 0.0057$                     | 5.6               | 150.0              | $0.1467 \pm 0.0076$                     | 5.5               |
|                     | 16.0          | 275.0              | $0.0011\pm0.0003$                       | 6.1               | 275.0              | $0.0058 \pm 0.0006$                     | 7.2               |
| 1.643               | -8.0          | -148.0             | $0.2950 \pm 0.0320$                     | 5.5               | -146.0             | $0.5160 \pm 0.0370$                     | 5.5               |
|                     | 8.0           | 148.0              | $0.5250\pm0.0310$                       | 5.5               | 146.0              | $1.0390\pm0.0360$                       | 5.4               |
| 2.442               | -20.0         | -355.0             | $0.0023 \pm 0.0011$                     | 5.5               | -355.0             | $0.0054 \pm 0.0011$                     | 5.4               |
|                     | -16.0         | -279.0             | $0.0143\pm0.0029$                       | 5.7               | -275.0             | $0.0288\pm0.0051$                       | 6.1               |
|                     | -8.0          | -149.0             | $0.9060 \pm 0.0260$                     | 5.5               | -149.0             | $1.5740\pm0.0374$                       | 5.5               |
|                     | -2.5          | -60.0              | $1.5981\pm0.0456$                       | 5.4               | -60.0              | $2.2360\pm0.0540$                       | 5.5               |
|                     | 2.5           | 60.0               | $1.5380 \pm 0.0513$                     | 5.4               | 60.0               | $2.6210 \pm 0.0650$                     | 5.5               |
|                     | 8.0           | 149.0              | $1.4605 \pm 0.0261$                     | 5.5               | 149.0              | $2.9950 \pm 0.0374$                     | 5.5               |
|                     | 16.0          | 279.0              | $0.0303\pm0.0029$                       | 5.7               | 276.0              | $0.1672\pm0.0051$                       | 6.2               |
|                     | 20.0          | 330.0              | $0.0057\pm0.0005$                       | 5.6               | 330.0              | $0.0214\pm0.0008$                       | 5.5               |

## b. Higher missing energies

Cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm miss}>20$  MeV are presented in Tables XIII - XXII.

TABLE XIII: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=0.843$  GeV,  $\theta_{pq}=0.0^{\circ},$  and  $E_{\rm miss}>25$  MeV. The  $P_{\rm miss}$  bins were 5 MeV/c wide. Cuts were applied to remove the radiative tail from  $^{1}{\rm H}(e,ep).$  While the HRSh was aligned along  $\vec{q},$  this data set does not truly correspond to parallel kinematics because of these cuts. Since  $\vec{p}_{p}$  and  $\vec{q}$  had about the same magnitude,  $\vec{P}_{\rm miss}$  arose from the slight angles between them, not from differences in their magnitudes. However, since the distribution of  $\vec{P}_{\rm miss}$  was symmetrical about  $\vec{q},$  the conditions of parallel kinematics are closely approximated. There is a 5.8% systematic uncertainty associated with these results.

| $E_{\rm miss}$ | $<\omega>$ | $< Q^{2} >$        | $< P_{\rm miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$ |
|----------------|------------|--------------------|--------------------|--|
| (MeV)          | (MeV)      | $(\text{GeV}/c)^2$ | (MeV/c)            | $(\text{nb/MeV}^2/\text{sr}^2)$              |
| 27.5           | 445.2      | 0.796              | 38.7               | $0.0024 \pm 0.0005$                          |
| 32.5           | 445.2      | 0.795              | 41.8               | $0.0085 \pm 0.0008$                          |
| 37.5           | 445.8      | 0.794              | 45.0               | $0.0097 \pm 0.0008$                          |
| 42.5           | 446.3      | 0.793              | 48.5               | $0.0113 \pm 0.0009$                          |
| 47.5           | 447.7      | 0.790              | 51.3               | $0.0106 \pm 0.0010$                          |
| 52.5           | 449.7      | 0.786              | 53.2               | $0.0065 \pm 0.0010$                          |
| 57.5           | 451.7      | 0.782              | 55.5               | $0.0062 \pm 0.0013$                          |

TABLE XIV: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=0.843$  GeV,  $\theta_{pq}=8.0^{\circ},$  and  $E_{\rm miss}>25$  MeV. The  $P_{\rm miss}$  bins were 5 MeV/c wide. There is a 6.0% systematic uncertainty associated with these results.

| $E_{ m miss}$ | $<\omega>$ | $< Q^{2} >$          | $< P_{\rm miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$ |
|---------------|------------|----------------------|--------------------|--|
| (MeV)         | (MeV)      | $(\mathrm{GeV}/c)^2$ | (MeV/c)            | $(\text{nb/MeV}^2/\text{sr}^2)$              |
| 25.5          | 444.9      | 0.796                | 143.3              | $0.0048 \pm 0.0013$                          |
| 26.5          | 444.6      | 0.796                | 143.5              | $0.0019 \pm 0.0010$                          |
| 27.5          | 445.2      | 0.795                | 143.8              | $0.0008 \pm 0.0009$                          |
| 28.5          | 444.8      | 0.796                | 143.5              | $0.0041 \pm 0.0011$                          |
| 29.5          | 444.6      | 0.796                | 143.9              | $0.0024 \pm 0.0010$                          |
| 30.5          | 444.7      | 0.796                | 143.9              | $0.0022 \pm 0.0009$                          |
| 31.5          | 444.9      | 0.796                | 144.2              | $0.0022 \pm 0.0009$                          |
| 32.5          | 444.8      | 0.796                | 144.0              | $0.0041 \pm 0.0010$                          |
| 33.5          | 445.0      | 0.795                | 144.6              | $0.0023 \pm 0.0009$                          |
| 34.5          | 445.0      | 0.795                | 144.5              | $0.0013 \pm 0.0008$                          |
| 35.5          | 444.9      | 0.796                | 144.7              | $0.0031 \pm 0.0009$                          |
| 36.5          | 445.0      | 0.796                | 145.0              | $0.0018 \pm 0.0008$                          |
| 37.5          | 445.1      | 0.796                | 145.1              | $0.0042 \pm 0.0010$                          |
| 38.5          | 444.9      | 0.796                | 145.9              | $0.0013 \pm 0.0008$                          |
| 39.5          | 444.9      | 0.796                | 145.6              | $0.0038 \pm 0.0010$                          |
| 40.5          | 445.0      | 0.796                | 146.2              | $0.0027 \pm 0.0009$                          |
| 41.5          | 444.9      | 0.796                | 146.2              | $0.0030 \pm 0.0008$                          |
| 42.5          | 445.1      | 0.795                | 146.4              | $0.0029 \pm 0.0009$                          |
| 43.5          | 445.1      | 0.795                | 147.3              | $0.0016 \pm 0.0008$                          |
| 44.5          | 444.6      | 0.796                | 147.1              | $0.0020 \pm 0.0008$                          |
| 45.5          | 445.4      | 0.795                | 147.6              | $0.0023 \pm 0.0008$                          |
| 46.5          | 446.1      | 0.793                | 147.8              | $0.0028 \pm 0.0009$                          |
| 47.5          | 446.5      | 0.793                | 148.0              | $0.0040 \pm 0.0010$                          |
| 48.5          | 447.1      | 0.791                | 148.4              | $0.0016 \pm 0.0009$                          |
| 49.5          | 447.5      | 0.790                | 148.5              | $0.0033 \pm 0.0010$                          |
| 50.5          | 448.0      | 0.789                | 149.3              | $0.0029 \pm 0.0010$                          |
| 51.5          | 448.5      | 0.789                | 149.5              | $0.0015 \pm 0.0009$                          |
| 52.5          | 449.0      | 0.787                | 149.8              | $0.0013 \pm 0.0007$                          |
| 53.5          | 449.4      | 0.786                | 150.0              | $0.0024 \pm 0.0007$                          |
| 54.5          | 450.0      | 0.785                | 151.1              | $0.0022 \pm 0.0009$                          |
| 55.5          | 450.5      | 0.784                | 151.2              | $0.0008 \pm 0.0008$                          |
| 56.5          | 451.1      | 0.783                | 151.7              | $0.0019 \pm 0.0010$                          |
| 57.5          | 451.6      | 0.782                | 151.7              | $0.0010 \pm 0.0010$                          |
| 58.5          | 452.0      | 0.782                | 152.7              | $0.0007 \pm 0.0009$                          |
| 59.5          | 452.5      | 0.781                | 152.6              | $0.0016 \pm 0.0011$                          |

TABLE XV: Measured cross sections for QE proton knockout from  $^{16}\,\mathrm{O}$  for  $E_{\mathrm{beam}}=0.843$  GeV,  $\theta_{pq}=16.0^{\circ},$  and  $E_{\mathrm{miss}}>25$  MeV. The  $P_{\mathrm{miss}}$  bins were 5 MeV/c wide. There is a 5.9% systematic uncertainty associated with these results.

| $E_{\rm miss}$ | $<\omega>$ | $< Q^{2} >$        | $< P_{\rm miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$ |
|----------------|------------|--------------------|--------------------|--|
| (MeV)          | (MeV)      | $(\text{GeV}/c)^2$ | (MeV/c)            | $(\text{nb/MeV}^2/\text{sr}^2)$              |
| 27.5           | 446.0      | 0.795              | 281.6              | $0.0004 \pm 0.0001$                          |
| 32.5           | 446.0      | 0.795              | 281.3              | $0.0003 \pm 0.0001$                          |
| 37.5           | 445.9      | 0.795              | 281.2              | $0.0003 \pm 0.0001$                          |
| 42.5           | 446.1      | 0.795              | 281.0              | $0.0002 \pm 0.0001$                          |
| 47.5           | 448.1      | 0.790              | 281.8              | $0.0002 \pm 0.0001$                          |
| 52.5           | 450.5      | 0.786              | 282.6              | $0.0003 \pm 0.0001$                          |
| 57.5           | 452.8      | 0.781              | 283.6              | $0.0002 \pm 0.0001$                          |

TABLE XVI: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=1.643$  GeV,  $\theta_{pq}=0.0^{\circ},$  and  $E_{\rm miss}>25$  MeV. The  $P_{\rm miss}$  bins were 5 MeV/c wide. Cuts were applied to remove the radiative tail from  $^1{\rm H}(e,ep)$ . While the HRS\_h was aligned along  $\vec{q},$  this data set does not truly correspond to parallel kinematics because of these cuts. Since  $\vec{p}_p$  and  $\vec{q}$  had about the same magnitude,  $\vec{P}_{\rm miss}$  arose from the slight angles between them, not from differences in their magnitudes. However, since the distribution of  $\vec{P}_{\rm miss}$  was symmetrical about  $\vec{q},$  the conditions of parallel kinematics are closely approximated. There is a 5.8% systematic uncertainty associated with these results.

| $E_{\rm miss}$ | < ω > | $\langle O^2 \rangle$ | $< P_{\rm miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$ |
|----------------|-------|-----------------------|--------------------|--|
| (MeV)          | (MeV) | $(\text{GeV}/c)^2$    | (MeV/c)            | $(\text{nb/MeV}^2/\text{sr}^2)$              |
| 27.5           | 450.0 | 0.795                 | 62.5               | $0.0195 \pm 0.0013$                          |
| 32.5           | 450.0 | 0.795                 | 62.5               | $0.0293 \pm 0.0012$                          |
| 37.5           | 450.0 | 0.795                 | 62.5               | $0.0483 \pm 0.0013$                          |
| 42.5           | 450.0 | 0.795                 | 62.5               | $0.0534 \pm 0.0014$                          |
| 47.5           | 450.0 | 0.795                 | 62.5               | $0.0445 \pm 0.0014$                          |
| 52.5           | 450.0 | 0.795                 | 65.0               | $0.0263 \pm 0.0015$                          |
| 57.5           | 450.0 | 0.795                 | 67.5               | $0.0132 \pm 0.0021$                          |

TABLE XVII: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=1.643~{\rm GeV},~|\theta_{pq}|=8.0^{\circ},~{\rm and}~E_{\rm miss}>25~{\rm MeV}.$  The  $P_{\rm miss}$  bins were 5 MeV/c wide. There is a 6.0% systematic uncertainty associated with these results.

|                     |                  |                      |                    | $\theta_{pq} = +8.0^{\circ}$  |                    | $\theta_{na} = -8.0^{\circ}$  |
|---------------------|------------------|----------------------|--------------------|---|--------------------|---|
| $E_{ m miss}$       | $<\omega>$       | $< Q^2 >$            | $< P_{\rm miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$                          | $< P_{\rm miss} >$ | F 1   |
| (MeV)               | (MeV)            | $(\mathrm{GeV}/c)^2$ | (MeV/c)            | $(\text{nb/MeV}^2/\text{sr}^2)$                                       | (MeV/c)            | $(\text{nb/MeV}^2/\text{sr}^2)$                                       |
| 25.5                | 436.2            | 0.804                | 141.8              | $0.0361 \pm 0.0036$   | 153.2              | $0.0163 \pm 0.0020$   |
| 26.5                | 438.0            | 0.802                | 142.7              | $0.0231 \pm 0.0031$   | 152.2              | $0.0130 \pm 0.0018$   |
| $27.5 \\ 28.5$      | $439.0 \\ 439.5$ | $0.802 \\ 0.802$     | $144.1 \\ 144.9$   | $0.0193 \pm 0.0029$<br>$0.0138 \pm 0.0026$                            | 151.7 $150.5$      | $0.0079 \pm 0.0016$<br>$0.0060 \pm 0.0015$                            |
| $\frac{26.5}{29.5}$ | 439.3 $441.2$    | 0.802                | 144.9              | $0.0138 \pm 0.0026$<br>$0.0167 \pm 0.0026$                            | 149.7              | $0.0000 \pm 0.0013$<br>$0.0117 \pm 0.0016$                            |
| 30.5                | 441.7            | 0.800                | 146.8              | $0.0209 \pm 0.0027$   | 148.8              | $0.0117 \pm 0.0016$<br>$0.0132 \pm 0.0016$                            |
| 31.5                | 442.4            | 0.801                | 147.5              | $0.0157 \pm 0.0025$   | 147.4              | $0.0101 \pm 0.0015$   |
| 32.5                | 443.6            | 0.799                | 148.8              | $0.0201 \pm 0.0026$   | 147.2              | $0.0075 \pm 0.0014$   |
| 33.5                | 445.1            | 0.798                | 149.9              | $0.0185 \pm 0.0026$   | 146.1              | $0.0098 \pm 0.0014$   |
| 34.5                | 445.8            | 0.796                | 151.3              | $0.0171 \pm 0.0025$   | 144.6              | $0.0138 \pm 0.0015$   |
| $35.5 \\ 36.5$      | $446.9 \\ 447.5$ | $0.796 \\ 0.796$     | 151.1 $151.9$      | $\begin{array}{c} 0.0178 \pm 0.0025 \\ 0.0226 \pm 0.0026 \end{array}$ | $144.3 \\ 144.0$   | $\begin{array}{c} 0.0109 \pm 0.0015 \\ 0.0135 \pm 0.0015 \end{array}$ |
| 37.5                | 448.9            | 0.795                | 153.8              | $0.0220 \pm 0.0020$<br>$0.0218 \pm 0.0025$                            | 144.0 $142.7$      | $0.0133 \pm 0.0013$<br>$0.0128 \pm 0.0015$                            |
| 38.5                | 450.0            | 0.796                | 154.5              | $0.0245 \pm 0.0027$   | 141.7              | $0.0139 \pm 0.0016$   |
| 39.5                | 450.6            | 0.795                | 155.1              | $0.0214 \pm 0.0026$   | 140.9              | $0.0151 \pm 0.0016$   |
| 40.5                | 451.5            | 0.795                | 156.0              | $0.0242 \pm 0.0027$   | 141.1              | $0.0128 \pm 0.0015$   |
| 41.5                | 452.0            | 0.793                | 156.6              | $0.0264 \pm 0.0027$   | 139.6              | $0.0144 \pm 0.0016$   |
| 42.5                | 453.7            | 0.792                | 158.1              | $0.0171 \pm 0.0025$   | 137.9              | $0.0173 \pm 0.0017$   |
| $43.5 \\ 44.5$      | 454.9 $456.3$    | $0.791 \\ 0.791$     | 159.3 $160.9$      | $\begin{array}{c} 0.0175 \pm 0.0024 \\ 0.0202 \pm 0.0025 \end{array}$ | 137.9 $136.6$      | $\begin{array}{c} 0.0144 \pm 0.0016 \\ 0.0142 \pm 0.0016 \end{array}$ |
| 45.5                | 456.6            | 0.791                | 160.9              | $0.0202 \pm 0.0025$<br>$0.0203 \pm 0.0025$                            | 135.5              | $0.0142 \pm 0.0016$<br>$0.0166 \pm 0.0016$                            |
| 46.5                | 457.4            | 0.789                | 161.3              | $0.0136 \pm 0.0022$   | 136.3              | $0.0149 \pm 0.0016$   |
| 47.5                | 459.0            | 0.788                | 162.5              | $0.0146 \pm 0.0022$   | 134.5              | $0.0162 \pm 0.0016$   |
| 48.5                | 459.9            | 0.788                | 163.7              | $0.0170 \pm 0.0023$   | 133.7              | $0.0127 \pm 0.0015$   |
| 49.5                | 461.1            | 0.787                | 164.6              | $0.0144 \pm 0.0022$   | 132.8              | $0.0125 \pm 0.0015$   |
| 50.5                | 462.3            | 0.787                | 165.6              | $0.0157 \pm 0.0023$   | 132.5              | $0.0138 \pm 0.0016$   |
| 51.5                | 462.8            | 0.786                | $166.4 \\ 168.0$   | $0.0142 \pm 0.0021$   | 131.9              | $0.0110 \pm 0.0015$<br>$0.0130 \pm 0.0015$                            |
| $52.5 \\ 53.5$      | $464.5 \\ 464.6$ | $0.785 \\ 0.785$     | 168.4              | $\begin{array}{c} 0.0079 \pm 0.0019 \\ 0.0078 \pm 0.0019 \end{array}$ | 130.2 $130.8$      | $0.0130 \pm 0.0013$<br>$0.0093 \pm 0.0014$                            |
| 54.5                | 465.5            | 0.784                | 169.3              | $0.0073 \pm 0.0013$<br>$0.0073 \pm 0.0018$                            | 130.1              | $0.0033 \pm 0.0014$<br>$0.0112 \pm 0.0014$                            |
| 55.5                | 466.4            | 0.785                | 170.1              | $0.0096 \pm 0.0019$   | 129.7              | $0.0109 \pm 0.0015$   |
| 56.5                | 467.0            | 0.784                | 170.5              | $0.0094 \pm 0.0019$   | 128.3              | $0.0069 \pm 0.0013$   |
| 57.5                | 467.3            | 0.783                | 171.1              | $0.0066 \pm 0.0018$   | 128.4              | $0.0078 \pm 0.0013$   |
| 58.5                | 468.2            | 0.783                | 171.0              | $0.0062 \pm 0.0018$   | 129.5              | $0.0070 \pm 0.0013$   |
| 59.5                | 468.3            | 0.782                | 171.8              | $0.0041 \pm 0.0016$   | 127.2              | $0.0097 \pm 0.0014$   |
| $60.5 \\ 61.5$      | $469.2 \\ 469.3$ | $0.782 \\ 0.782$     | 173.1 $172.9$      | $\begin{array}{c} 0.0100 \pm 0.0019 \\ 0.0060 \pm 0.0018 \end{array}$ | 127.8 $127.1$      | $\begin{array}{c} 0.0070 \pm 0.0013 \\ 0.0036 \pm 0.0012 \end{array}$ |
| 62.5                | 470.6            | 0.782                | 173.9              | $0.0000 \pm 0.0018$<br>$0.0051 \pm 0.0018$                            | 127.3              | $0.0030 \pm 0.0012$<br>$0.0085 \pm 0.0014$                            |
| 63.5                | 469.9            | 0.782                | 173.6              | $0.0062 \pm 0.0017$   | 126.8              | $0.0040 \pm 0.0012$   |
| 64.5                | 471.0            | 0.781                | 174.7              | $0.0071 \pm 0.0019$   | 126.9              | $0.0065 \pm 0.0013$   |
| 65.5                | 471.2            | 0.780                | 174.5              | $0.0045 \pm 0.0018$   | 125.8              | $0.0043 \pm 0.0013$   |
| 66.5                | 472.1            | 0.779                | 175.5              | $0.0077 \pm 0.0019$   | 125.9              | $0.0056 \pm 0.0013$   |
| 67.5                | 472.6            | 0.780                | 175.9              | $0.0049 \pm 0.0019$   | 125.5              | $0.0019 \pm 0.0012$   |
| $68.5 \\ 69.5$      | 473.4 $473.3$    | 0.779 $0.779$        | $177.2 \\ 177.0$   | $0.0061 \pm 0.0019$<br>$0.0071 \pm 0.0019$                            | 126.1 $124.0$      | $\begin{array}{c} 0.0049 \pm 0.0013 \\ 0.0022 \pm 0.0012 \end{array}$ |
| 70.5                | 473.3 $474.4$    | 0.778                | 177.9              | $0.0071 \pm 0.0019$<br>$0.0020 \pm 0.0017$                            | 125.2              | $0.0022 \pm 0.0012$<br>$0.0056 \pm 0.0013$                            |
| 71.5                | 474.5            | 0.779                | 178.7              | $0.0023 \pm 0.0017$<br>$0.0033 \pm 0.0017$                            | 124.8              | $0.0034 \pm 0.0013$   |
| 72.5                | 474.9            | 0.778                | 178.4              | $0.0052 \pm 0.0018$   | 125.2              | $0.0066 \pm 0.0015$   |
| 73.5                | 475.1            | 0.778                | 179.0              | $0.0065 \pm 0.0020$   | 125.1              | $0.0046 \pm 0.0014$   |
| 74.5                | 476.3            | 0.777                | 179.6              | $0.0027 \pm 0.0018$   | 124.4              | $0.0032 \pm 0.0013$   |
| 75.5                | 476.2            | 0.776                | 180.3              | $0.0026 \pm 0.0017$   | 124.4              | $0.0046 \pm 0.0014$   |
| 76.5                | 477.1            | 0.776                | 181.4              | $0.0061 \pm 0.0021$   | 122.3              | $0.0005 \pm 0.0012$   |
| $77.5 \\ 78.5$      | 477.6 $478.2$    | $0.776 \\ 0.777$     | $181.7 \\ 182.7$   | $0.0034 \pm 0.0019$<br>$0.0056 \pm 0.0021$                            | 124.1 $123.8$      | $\begin{array}{c} 0.0016 \pm 0.0013 \\ 0.0013 \pm 0.0014 \end{array}$ |
| 79.5                | 478.9            | 0.775                | 183.1              | $0.0056 \pm 0.0021$<br>$0.0056 \pm 0.0021$                            | 123.4              | $0.0013 \pm 0.0014$<br>$0.0054 \pm 0.0016$                            |
| 80.5                | 479.1            | 0.774                | 183.3              | $0.0059 \pm 0.0023$   | 122.9              | $0.0040 \pm 0.0016$   |
| 81.5                | 479.6            | 0.776                | 184.1              | $0.0008\pm0.0018$   | 122.7              | $0.0039 \pm 0.0017$   |
| 82.5                | 480.1            | 0.775                | 185.1              | $0.0007 \pm 0.0018$   | 122.8              | $0.0029 \pm 0.0016$   |
| 83.5                | 480.6            | 0.776                | 185.2              | $0.0039 \pm 0.0021$   | 121.8              | $0.0022 \pm 0.0016$   |
| 84.5                | 481.1            | 0.773                | 185.8              | $0.0058 \pm 0.0025$   | 122.8              | $\begin{array}{c} 0.0018 \pm 0.0016 \\ 0.0039 \pm 0.0019 \end{array}$ |
| $85.5 \\ 86.5$      | $481.6 \\ 482.1$ | $0.775 \\ 0.775$     | 186.3 $187.1$      | $\begin{array}{c} 0.0028 \pm 0.0023 \\ 0.0065 \pm 0.0027 \end{array}$ | 122.2 $122.9$      | $0.0039 \pm 0.0019$<br>$0.0003 \pm 0.0018$                            |
| 87.5                | 482.1            | 0.772                | 187.6              | $0.0003 \pm 0.0027$<br>$0.0049 \pm 0.0030$                            | 123.1              | $0.0003 \pm 0.0018$<br>$0.0029 \pm 0.0021$                            |
|                     |                  | <b>.</b>             |                    | 0.0000  |                    | 5.5525 <u>T</u> 0.00 <u>2</u> 1                                       |

TABLE XVIII: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=2.442$  GeV,  $\theta_{pq}=0.0^{\circ},$  and  $E_{\rm miss}>25$  MeV. The  $P_{\rm miss}$  bins were 5 MeV/c wide. Cuts were applied to remove the radiative tail from  $^{1}{\rm H}(e,ep).$  While the  ${\rm HRS}_h$  was aligned along  $\vec{q},$  this data set does not truly correspond to parallel kinematics because of these cuts. Since  $\vec{p}_p$  and  $\vec{q}$  had about the same magnitude,  $\vec{P}_{\rm miss}$  arose from the slight angles between them, not from differences in their magnitudes. However, since the distribution of  $\vec{P}_{\rm miss}$  was symmetrical about  $\vec{q},$  the conditions of parallel kinematics are closely approximated. There is a 5.8% systematic uncertainty associated with these results.

| E             | Z          | < 02 >               | < D >                          | 16 _ / 1 1F _ 1O _ 1O                        |
|---------------|------------|----------------------|--------------------------------|--|
| $E_{ m miss}$ | $<\omega>$ | < \Q >               | $\langle P_{\rm miss} \rangle$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$ |
| (MeV)         | (MeV)      | $(\mathrm{GeV}/c)^2$ | (MeV/c)                        | $(\text{nb/MeV}^2/\text{sr}^2)$              |
| 27.5          | 450.0      | 0.795                | 60.0                           | $0.0552 \pm 0.0042$                          |
| 32.5          | 450.0      | 0.795                | 60.0                           | $0.0890 \pm 0.0045$                          |
| 37.5          | 450.0      | 0.795                | 60.0                           | $0.1387 \pm 0.0050$                          |
| 42.5          | 450.0      | 0.795                | 60.0                           | $0.1580 \pm 0.0058$                          |
| 47.5          | 450.0      | 0.795                | 62.5                           | $0.1348 \pm 0.0062$                          |
| 52.5          | 450.0      | 0.795                | 65.0                           | $0.0756 \pm 0.0063$                          |
| 57.5          | 450.0      | 0.795                | 67.5                           | $0.0402 \pm 0.0084$                          |

TABLE XIX: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=2.442~{\rm GeV},~\theta_{pq}=-2.5^{\circ},$  and  $E_{\rm miss}>25~{\rm MeV}.$  The  $P_{\rm miss}$  bins were 5 MeV/c wide. There is a 5.9% systematic uncertainty associated with these results.

|               |            | - 11                 | 1                  | E .  |
|---------------|------------|----------------------|--------------------|--|
| $E_{ m miss}$ | $<\omega>$ | $< Q^2 >$            | $< P_{\rm miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$ |
| (MeV)         | (MeV)      | $(\mathrm{GeV}/c)^2$ | (MeV/c)            | $(\text{nb/MeV}^2/\text{sr}^2)$              |
| 25.5          | 445.0      | 0.823                | 46.5               | $0.0330 \pm 0.0182$                          |
| 26.5          | 446.5      | 0.822                | 46.8               | $0.0661 \pm 0.0185$                          |
| 27.5          | 449.5      | 0.821                | 46.7               | $0.0388 \pm 0.0173$                          |
| 28.5          | 449.3      | 0.820                | 45.3               | $0.0590 \pm 0.0176$                          |
| 29.5          | 450.4      | 0.823                | 46.2               | $0.0955 \pm 0.0192$                          |
| 30.5          | 450.8      | 0.823                | 45.0               | $0.0589 \pm 0.0181$                          |
| 31.5          | 451.9      | 0.821                | 45.4               | $0.0733 \pm 0.0180$                          |
| 32.5          | 452.1      | 0.823                | 45.0               | $0.0810 \pm 0.0179$                          |
| 33.5          | 453.3      | 0.822                | 45.6               | $0.0944 \pm 0.0192$                          |
| 34.5          | 454.5      | 0.821                | 45.2               | $0.1375 \pm 0.0211$                          |
| 35.5          | 455.1      | 0.821                | 46.1               | $0.0984 \pm 0.0209$                          |
| 36.5          | 454.9      | 0.822                | 46.1               | $0.1950 \pm 0.0227$                          |
| 37.5          | 457.3      | 0.821                | 45.6               | $0.1566 \pm 0.0232$                          |
| 38.5          | 458.4      | 0.820                | 45.8               | $0.1937 \pm 0.0232$                          |
| 39.5          | 458.4      | 0.820                | 46.1               | $0.2052 \pm 0.0251$                          |
| 40.5          | 459.3      | 0.821                | 46.5               | $0.1841 \pm 0.0236$                          |
| 41.5          | 459.9      | 0.819                | 45.8               | $0.2354 \pm 0.0252$                          |
| 42.5          | 461.3      | 0.818                | 45.9               | $0.2401 \pm 0.0260$                          |
| 43.5          | 462.7      | 0.817                | 45.6               | $0.1791 \pm 0.0247$                          |
| 44.5          | 462.6      | 0.818                | 46.6               | $0.2049 \pm 0.0245$                          |
| 45.5          | 464.0      | 0.816                | 45.9               | $0.1401 \pm 0.0223$                          |
| 46.5          | 464.7      | 0.816                | 46.9               | $0.1721 \pm 0.0224$                          |
| 47.5          | 467.9      | 0.817                | 45.7               | $0.1457 \pm 0.0217$                          |
| 48.5          | 467.7      | 0.816                | 45.9               | $0.1323 \pm 0.0211$                          |
| 49.5          | 468.2      | 0.815                | 45.8               | $0.1469 \pm 0.0211$                          |
| 50.5          | 471.1      | 0.814                | 45.3               | $0.0893 \pm 0.0189$                          |
| 51.5          | 471.0      | 0.814                | 45.9               | $0.1008 \pm 0.0185$                          |
| 52.5          | 473.1      | 0.814                | 46.3               | $0.0866 \pm 0.0175$                          |
| 53.5          | 472.1      | 0.813                | 45.8               | $0.1037 \pm 0.0183$                          |
| 54.5          | 474.6      | 0.813                | 45.7               | $0.0607 \pm 0.0165$                          |
| 55.5          | 474.5      | 0.812                | 45.4               | $0.0766 \pm 0.0163$                          |
| 56.5          | 473.8      | 0.810                | 46.8               | $0.0617 \pm 0.0155$                          |
| 57.5          | 476.5      | 0.810                | 45.8               | $0.0606 \pm 0.0155$                          |
| 58.5          | 477.4      | 0.811                | 46.6               | $0.0717 \pm 0.0158$                          |
| 59.5          | 479.4      | 0.809                | 45.1               | $0.0837 \pm 0.0168$                          |
| 60.5          | 481.5      | 0.810                | 45.5               | $0.0298 \pm 0.0140$                          |
| 61.5          | 480.8      | 0.807                | 46.2               | $0.0748 \pm 0.0156$                          |
| 62.5          | 480.6      | 0.807                | 47.7               | $0.0165 \pm 0.0125$                          |
| 63.5          | 480.7      | 0.805                | 47.8               | $0.0240 \pm 0.0118$                          |
| 64.5          | 481.1      | 0.805                | 47.6               | $0.0135 \pm 0.0109$                          |
| 65.5          | 484.1      | 0.805                | 46.5               | $0.0471 \pm 0.0127$                          |
| 66.5          | 482.4      | 0.804                | 46.6               | $0.0195 \pm 0.0118$                          |
| 67.5          | 485.9      | 0.804                | 47.4               | $0.0297 \pm 0.0121$                          |
| 68.5          | 484.4      | 0.803                | 48.7               | $0.0491 \pm 0.0134$                          |
| 69.5          | 490.6      | 0.802                | 46.5               | $0.0118 \pm 0.0116$                          |
| 70.5          | 489.5      | 0.800                | 47.6               | $0.0021 \pm 0.0103$                          |
| 71.5          | 490.8      | 0.800                | 48.3               | $0.0136 \pm 0.0103$                          |
| 72.5          | 491.7      | 0.800                | 47.9               | $0.0306 \pm 0.0118$                          |
| 73.5          | 491.6      | 0.799                | 49.2               | $0.0156 \pm 0.0113$                          |
| 74.5          | 493.1      | 0.797                | 49.6               | $0.0192 \pm 0.0114$                          |
| 75.5          | 494.7      | 0.798                | 49.1               | $0.0040 \pm 0.0101$                          |
| 76.5          | 493.8      | 0.797                | 49.2               | $0.0144 \pm 0.0111$                          |
| 77.5          | 496.0      | 0.795                | 48.7               | $0.0098 \pm 0.0118$                          |
| 78.5          | 497.2      | 0.794                | 48.8               | $-0.0039 \pm 0.0099$                         |
| 79.5          | 498.3      | 0.793                | 50.8               | $0.0103 \pm 0.0124$                          |

TABLE XX: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=2.442~{\rm GeV},~|\theta_{pq}|=8.0^{\circ},$  and  $E_{\rm miss}>25~{\rm MeV}.$  The  $P_{\rm miss}$  bins were 5 MeV/c wide. There is a 6.0% systematic uncertainty associated with these results.

|                     |                  |                      |                   | $\theta_{pq} = +8.0^{\circ}$  |                    | $\theta_{pq} = -8.0^{\circ}$  |
|---------------------|------------------|----------------------|-------------------|---|--------------------|---|
| $E_{ m miss}$       | $<\omega>$       | $< Q^{2} >$          | $< P_{ m miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$                          | $< P_{\rm miss} >$ | $d^6\sigma/d\omega dE_n d\Omega_e d\Omega_n$                          |
| (MeV)               | (MeV)            | $(\mathrm{GeV}/c)^2$ | (MeV/c)           | $(\text{nb/MeV}^2/\text{sr}^2)$                                       | $(\mathrm{MeV}/c)$ | $(nb/MeV^2/sr^2)$   |
| 25.5                | 438.1            | 0.793                | 150.0             | $0.0595 \pm 0.0058$   | 160.0              | $0.0174 \pm 0.0030$   |
| 26.5                | 439.6            | 0.791                | 152.5             | $0.0310 \pm 0.0051$   | 160.0              | $0.0165 \pm 0.0027$   |
| $27.5 \\ 28.5$      | $440.5 \\ 441.7$ | $0.791 \\ 0.789$     | 155.0 $155.0$     | $\begin{array}{c} 0.0371 \pm 0.0049 \\ 0.0474 \pm 0.0050 \end{array}$ | 155.2 $157.9$      | $\begin{array}{c} 0.0190 \pm 0.0026 \\ 0.0249 \pm 0.0027 \end{array}$ |
| 29.5                | 442.3            | 0.789                | 152.8             | $0.0566 \pm 0.0051$   | 155.2              | $0.0306 \pm 0.0028$   |
| 30.5                | 443.4            | 0.788                | 155.0             | $0.0412 \pm 0.0048$   | 157.5              | $0.0221 \pm 0.0027$   |
| 31.5                | 444.4            | 0.792                | 157.5             | $0.0492 \pm 0.0048$   | 155.0              | $0.0318 \pm 0.0028$   |
| 32.5                | 446.6            | 0.788                | 160.0             | $0.0545 \pm 0.0048$   | 155.0              | $0.0247 \pm 0.0027$   |
| $33.5 \\ 34.5$      | $447.8 \\ 448.0$ | $0.789 \\ 0.788$     | 160.0<br>160.0    | $0.0450 \pm 0.0047$<br>$0.0498 \pm 0.0047$                            | $155.0 \\ 152.7$   | $\begin{array}{c} 0.0289 \pm 0.0027 \\ 0.0291 \pm 0.0027 \end{array}$ |
| 35.5                | 449.5            | 0.784                | 160.0             | $0.0498 \pm 0.0047$<br>$0.0625 \pm 0.0049$                            | 150.0              | $0.0291 \pm 0.0027$<br>$0.0294 \pm 0.0027$                            |
| 36.5                | 449.1            | 0.784                | 160.0             | $0.0609 \pm 0.0049$   | 150.0              | $0.0309 \pm 0.0027$   |
| 37.5                | 452.1            | 0.786                | 162.5             | $0.0443 \pm 0.0046$   | 147.5              | $0.0357 \pm 0.0028$   |
| 38.5                | 452.7            | 0.788                | 162.5             | $0.0521 \pm 0.0046$   | 150.0              | $0.0413 \pm 0.0029$   |
| $\frac{39.5}{40.5}$ | $453.7 \\ 454.1$ | $0.785 \\ 0.783$     | 165.0 $165.0$     | $\begin{array}{c} 0.0459 \pm 0.0045 \\ 0.0537 \pm 0.0046 \end{array}$ | $147.9 \\ 145.2$   | $\begin{array}{c} 0.0336 \pm 0.0028 \\ 0.0359 \pm 0.0028 \end{array}$ |
| 40.5 $41.5$         | 454.1 $454.6$    | 0.784                | 165.0             | $0.0337 \pm 0.0040$<br>$0.0416 \pm 0.0044$                            | 147.5              | $0.0368 \pm 0.0028$<br>$0.0368 \pm 0.0028$                            |
| 42.5                | 456.7            | 0.783                | 165.0             | $0.0456 \pm 0.0044$   | 147.5              | $0.0431 \pm 0.0030$   |
| 43.5                | 456.9            | 0.782                | 167.8             | $0.0421 \pm 0.0043$   | 147.5              | $0.0350 \pm 0.0028$   |
| 44.5                | 457.3            | 0.780                | 170.0             | $0.0392 \pm 0.0042$   | 145.0              | $0.0382 \pm 0.0028$   |
| 45.5                | 457.8            | 0.784                | 167.5             | $0.0462 \pm 0.0043$   | 142.7              | $0.0335 \pm 0.0028$   |
| $\frac{46.5}{47.5}$ | 458.3 $459.8$    | $0.781 \\ 0.779$     | 170.0 $172.5$     | $\begin{array}{c} 0.0387 \pm 0.0042 \\ 0.0408 \pm 0.0042 \end{array}$ | $145.0 \\ 145.2$   | $\begin{array}{c} 0.0330 \pm 0.0028 \\ 0.0326 \pm 0.0027 \end{array}$ |
| 48.5                | 460.4            | 0.782                | 170.0             | $0.0317 \pm 0.0040$   | 142.7              | $0.0320 \pm 0.0027$<br>$0.0331 \pm 0.0027$                            |
| 49.5                | 461.6            | 0.783                | 175.0             | $0.0287 \pm 0.0039$   | 143.0              | $0.0217 \pm 0.0025$   |
| 50.5                | 463.6            | 0.779                | 172.8             | $0.0249 \pm 0.0037$   | 143.0              | $0.0274 \pm 0.0026$   |
| 51.5                | 463.5            | 0.780                | 175.0             | $0.0268 \pm 0.0037$   | 142.5              | $0.0257 \pm 0.0025$   |
| $52.5 \\ 53.5$      | $463.1 \\ 465.2$ | $0.784 \\ 0.778$     | 172.8 $172.5$     | $0.0208 \pm 0.0035$<br>$0.0170 \pm 0.0034$                            | $145.0 \\ 145.4$   | $\begin{array}{c} 0.0222 \pm 0.0025 \\ 0.0191 \pm 0.0024 \end{array}$ |
| 54.5                | 466.2            | 0.779                | 175.0             | $0.0170 \pm 0.0034$<br>$0.0249 \pm 0.0035$                            | 145.4              | $0.0191 \pm 0.0024$<br>$0.0214 \pm 0.0024$                            |
| 55.5                | 468.5            | 0.782                | 180.0             | $0.0147 \pm 0.0032$   | 145.0              | $0.0175 \pm 0.0023$   |
| 56.5                | 468.6            | 0.778                | 180.0             | $0.0211 \pm 0.0034$   | 143.4              | $0.0160 \pm 0.0022$   |
| 57.5                | 469.3            | 0.779                | 177.5             | $0.0144 \pm 0.0032$   | 140.5              | $0.0181 \pm 0.0022$   |
| $58.5 \\ 59.5$      | 471.3 $472.3$    | $0.774 \\ 0.778$     | 182.5<br>180.0    | $\begin{array}{c} 0.0131 \pm 0.0031 \\ 0.0147 \pm 0.0031 \end{array}$ | $142.5 \\ 142.7$   | $\begin{array}{c} 0.0149 \pm 0.0022 \\ 0.0145 \pm 0.0022 \end{array}$ |
| 60.5                | 472.3            | 0.778                | 177.5             | $0.0147 \pm 0.0031$<br>$0.0149 \pm 0.0031$                            | 145.0              | $0.0143 \pm 0.0022$<br>$0.0143 \pm 0.0021$                            |
| 61.5                | 474.9            | 0.780                | 185.0             | $0.0057 \pm 0.0028$   | 143.2              | $0.0131 \pm 0.0021$   |
| 62.5                | 473.8            | 0.781                | 185.0             | $0.0164 \pm 0.0030$   | 137.5              | $0.0156 \pm 0.0021$   |
| 63.5                | 475.9            | 0.784                | 187.5             | $0.0112 \pm 0.0029$   | 140.8              | $0.0087 \pm 0.0020$   |
| $64.5 \\ 65.5$      | $477.0 \\ 477.6$ | $0.783 \\ 0.784$     | 185.0<br>185.0    | $\begin{array}{c} 0.0127 \pm 0.0029 \\ 0.0085 \pm 0.0028 \end{array}$ | 137.8 $140.0$      | $\begin{array}{c} 0.0105 \pm 0.0020 \\ 0.0081 \pm 0.0019 \end{array}$ |
| 66.5                | 477.2            | 0.734 $0.777$        | 187.5             | $0.0083 \pm 0.0028$<br>$0.0142 \pm 0.0029$                            | 138.6              | $0.0081 \pm 0.0019$<br>$0.0089 \pm 0.0019$                            |
| 67.5                | 477.0            | 0.781                | 190.0             | $0.0111 \pm 0.0029$   | 135.6              | $0.0086 \pm 0.0019$   |
| 68.5                | 480.2            | 0.780                | 187.5             | $0.0114 \pm 0.0029$   | 137.5              | $0.0077 \pm 0.0018$   |
| 69.5                | 480.0            | 0.782                | 187.5             | $0.0061 \pm 0.0026$   | 135.0              | $0.0089 \pm 0.0019$   |
| $70.5 \\ 71.5$      | $481.1 \\ 481.7$ | $0.778 \\ 0.778$     | 190.0 $192.5$     | $0.0096 \pm 0.0027$<br>$0.0044 \pm 0.0025$                            | 138.0 $133.4$      | $\begin{array}{c} 0.0074 \pm 0.0018 \\ 0.0030 \pm 0.0016 \end{array}$ |
| 72.5                | 481.7            | 0.781                | 192.5             | $0.0051 \pm 0.0024$   | 138.0              | $0.0080 \pm 0.0018$   |
| 73.5                | 482.8            | 0.782                | 192.5             | $0.0133 \pm 0.0027$   | 134.6              | $0.0058 \pm 0.0018$   |
| 74.5                | 484.8            | 0.781                | 192.8             | $0.0097 \pm 0.0027$   | 137.5              | $0.0063 \pm 0.0018$   |
| 75.5                | 485.0            | 0.779                | 197.2             | $0.0046 \pm 0.0025$   | 136.4              | $0.0057 \pm 0.0017$   |
| $76.5 \\ 77.5$      | $484.6 \\ 485.5$ | $0.773 \\ 0.781$     | 195.0 $192.5$     | $\begin{array}{c} 0.0057 \pm 0.0025 \\ 0.0048 \pm 0.0024 \end{array}$ | $128.2 \\ 135.0$   | $\begin{array}{c} 0.0036 \pm 0.0016 \\ 0.0030 \pm 0.0016 \end{array}$ |
| 78.5                | 488.2            | 0.781                | 195.3             | $0.0040 \pm 0.0024$<br>$0.0054 \pm 0.0024$                            | 132.5              | $0.0030 \pm 0.0010$<br>$0.0070 \pm 0.0017$                            |
| 79.5                | 488.6            | 0.782                | 197.5             | $0.0026 \pm 0.0023$   | 132.5              | $0.0033 \pm 0.0016$   |
| 80.5                | 490.3            | 0.785                | 195.3             | $0.0104 \pm 0.0026$   | 133.1              | $0.0077 \pm 0.0017$   |
| 81.5                | 489.1            | 0.785                | 197.5             | $0.0035 \pm 0.0024$   | 132.5              | $0.0048 \pm 0.0017$   |
| $82.5 \\ 83.5$      | $492.5 \\ 492.3$ | $0.782 \\ 0.782$     | 197.8<br>197.5    | $\begin{array}{c} 0.0045 \pm 0.0023 \\ 0.0025 \pm 0.0023 \end{array}$ | 134.3 $135.3$      | $\begin{array}{c} 0.0043 \pm 0.0017 \\ 0.0027 \pm 0.0016 \end{array}$ |
| 84.5                | 492.6            | 0.778                | 200.0             | $0.0025 \pm 0.0025$<br>$0.0065 \pm 0.0024$                            | 127.5              | $0.0027 \pm 0.0010$<br>$0.0072 \pm 0.0017$                            |
| 85.5                | 495.2            | 0.787                | 200.0             | $0.0048 \pm 0.0024$   | 137.5              | $0.0024 \pm 0.0016$   |
| 86.5                | 495.6            | 0.790                | 202.5             | $0.0025 \pm 0.0023$   | 133.7              | $0.0021 \pm 0.0016$   |
| 87.5                | 498.7            | 0.787                | 200.0             | $0.0119 \pm 0.0026$   | 127.5              | $0.0021 \pm 0.0016$   |
| $88.5 \\ 89.5$      | 499.6 $497.7$    | $0.785 \\ 0.784$     | 200.0 $202.5$     | $\begin{array}{c} 0.0044 \pm 0.0025 \\ 0.0086 \pm 0.0026 \end{array}$ | 127.5 $130.3$      | $\begin{array}{c} 0.0033 \pm 0.0016 \\ 0.0008 \pm 0.0016 \end{array}$ |
| 90.5                | 497.8            | 0.781                | 202.5             | $0.0050 \pm 0.0026$<br>$0.0052 \pm 0.0026$                            | 133.1              | $0.0003 \pm 0.0010$<br>$0.0031 \pm 0.0017$                            |
| 91.5                | 499.1            | 0.782                | 202.5             | $0.0023 \pm 0.0024$   | 132.2              | $0.0029 \pm 0.0018$   |
| 92.5                | 500.8            | 0.789                | 202.5             | $0.0067 \pm 0.0026$   | 130.3              | $-0.0008 \pm 0.0016$  |
| 93.5                | 500.4            | 0.794                | 207.5             | $0.0060 \pm 0.0026$   | 132.8              | $0.0022 \pm 0.0017$   |
| $94.5 \\ 95.5$      | 498.8 $498.8$    | $0.779 \\ 0.775$     | $202.5 \\ 202.5$  | $\begin{array}{c} 0.0059 \pm 0.0026 \\ 0.0085 \pm 0.0028 \end{array}$ | 128.8 $131.2$      | $-0.0003 \pm 0.0017$<br>$0.0021 \pm 0.0017$                           |
| 96.5                | 499.6            | 0.773                | 205.0             | $0.0083 \pm 0.0028$<br>$0.0087 \pm 0.0028$                            | 127.5              | $0.0021 \pm 0.0017$<br>$0.0049 \pm 0.0019$                            |
| 97.5                | 499.2            | 0.790                | 210.0             | $0.0022 \pm 0.0026$   | 132.5              | $0.0038 \pm 0.0019$   |
| 98.5                | 501.6            | 0.782                | 205.0             | $0.0118 \pm 0.0031$   | 128.2              | $-0.0024 \pm 0.0015$  |
| 99.5                | 504.3 $503.0$    | 0.774                | 205.0<br>207.5    | $\begin{array}{c} 0.0080 \pm 0.0029 \\ 0.0031 \pm 0.0027 \end{array}$ | 125.7 $127.5$      | $\begin{array}{c} 0.0000 \pm 0.0017 \\ 0.0016 \pm 0.0019 \end{array}$ |
| 100.5 $101.5$       | 500.7            | $0.781 \\ 0.776$     | 207.5             | $0.0031 \pm 0.0027$<br>$0.0105 \pm 0.0031$                            | $127.5 \\ 126.7$   | $0.0016 \pm 0.0019$<br>$0.0008 \pm 0.0019$                            |
| 102.5               | 502.6            | 0.776                | 210.0             | $0.0021 \pm 0.0028$   | 125.4              | $0.0006 \pm 0.0018$   |
| 103.5               | 501.9            | 0.776                | 210.0             | $0.0030\pm0.0028$   | 130.0              | $-0.0013 \pm 0.0017$  |

| 4045  |       | 0 =00 |       | 0.0000   0.0001     | 1050  | 0.0010   0.0010      |
|-------|-------|-------|-------|---------------------|-------|----------------------|
| 104.5 | 504.8 | 0.780 | 207.5 | $0.0080 \pm 0.0031$ | 127.8 | $0.0016 \pm 0.0019$  |
| 105.5 | 503.6 | 0.774 | 210.0 | $0.0051 \pm 0.0031$ | 125.0 | $-0.0004 \pm 0.0018$ |
| 106.5 | 507.9 | 0.778 | 210.5 | $0.0000 \pm 0.0028$ | 129.0 | $-0.0027 \pm 0.0016$ |
| 107.5 | 507.1 | 0.784 | 210.0 | $0.0112 \pm 0.0034$ | 127.5 | $0.0048 \pm 0.0022$  |
| 108.5 | 509.3 | 0.781 | 212.5 | $0.0036 \pm 0.0032$ | 125.0 | $0.0033 \pm 0.0023$  |
| 109.5 | 510.0 | 0.781 | 212.5 | $0.0047 \pm 0.0032$ | 124.0 | $-0.0014 \pm 0.0019$ |
| 110.5 | 510.0 | 0.779 | 212.5 | $0.0020 \pm 0.0031$ | 126.1 | $0.0028 \pm 0.0022$  |
| 111.5 | 510.0 | 0.782 | 212.5 | $0.0024 \pm 0.0030$ | 122.5 | $-0.0007 \pm 0.0022$ |
| 112.5 | 510.0 | 0.779 | 212.5 | $0.0046 \pm 0.0033$ | 122.5 | $0.0025 \pm 0.0024$  |
| 113.5 | 510.0 | 0.769 | 216.4 | $0.0114 \pm 0.0038$ | 117.5 | $0.0029 \pm 0.0025$  |
| 114.5 | 510.0 | 0.778 | 215.0 | $0.0095 \pm 0.0040$ | 120.2 | $-0.0013 \pm 0.0021$ |
| 115.5 | 510.0 | 0.777 | 215.0 | $0.0048 \pm 0.0037$ | 122.5 | $-0.0015 \pm 0.0020$ |
| 116.5 | 510.0 | 0.776 | 215.8 | $0.0018 \pm 0.0034$ | 121.0 | $0.0005 \pm 0.0021$  |
| 117.5 | 510.0 | 0.774 | 215.0 | $0.0017 \pm 0.0033$ | 121.4 | $0.0017 \pm 0.0023$  |
| 118.5 | 510.0 | 0.759 | 217.5 | $0.0127 \pm 0.0045$ | 113.6 | $0.0016 \pm 0.0024$  |
| 119.5 | 510.0 | 0.777 | 217.5 | $0.0078 \pm 0.0046$ | 122.5 | $0.0018 \pm 0.0027$  |

TABLE XXI: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=2.442~{\rm GeV},~|\theta_{pq}|=16.0^{\circ},$  and  $E_{\rm miss}>25~{\rm MeV}.$  The  $P_{\rm miss}$  bins were 5 MeV/c wide. There is a 5.8% systematic uncertainty associated with these results.

|                         |                  |   | T                                 | 0 110.00   |   | 0 10.00  |
|-------------------------|------------------|---|-----------------------------------|--|---|--|
| r.                      |                  | $< Q^2 >$                                 | - D                               | $\theta_{pq} = +16.0^{\circ}$  | < D >                                     | $\theta_{pq} = -16.0^{\circ}$  |
| $E_{\text{miss}}$ (MeV) | $<\omega>$ (MeV) | $\langle Q \rangle$<br>$(\text{GeV}/c)^2$ | $\langle P_{\text{miss}} \rangle$ | $\frac{d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p}{(\text{nb/MeV}^2/\text{sr}^2)}$ | $\langle P_{\rm miss} \rangle$<br>(MeV/c) | $\frac{d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p}{(\text{nb/MeV}^2/\text{sr}^2)}$ |
| 25.5                    | 439.9            | 0.794                                     | (MeV/c) 268.9                     | $0.0078 \pm 0.0008$  | 282.1                                     | $0.0095 \pm 0.0020$  |
| 26.5                    | 440.0            | 0.788                                     | 273.8                             | $0.0076 \pm 0.0008$<br>$0.0076 \pm 0.0008$   | 278.1                                     | $0.0033 \pm 0.0020$<br>$0.0014 \pm 0.0019$   |
| $\frac{20.5}{27.5}$     | 443.6            | 0.799                                     | 274.9                             | $0.0070 \pm 0.0003$<br>$0.0053 \pm 0.0007$   | 280.4                                     | $0.0014 \pm 0.0013$<br>$0.0078 \pm 0.0020$   |
| 28.5                    | 444.8            | 0.788                                     | 275.8                             | $0.0054 \pm 0.0007$  | 276.0                                     | $0.0043 \pm 0.0020$  |
| 29.5                    | 447.2            | 0.789                                     | 277.7                             | $0.0075 \pm 0.0007$  | 278.0                                     | $0.0053 \pm 0.0021$  |
| 30.5                    | 444.0            | 0.799                                     | 278.9                             | $0.0054 \pm 0.0007$  | 279.0                                     | $0.0078 \pm 0.0021$  |
| 31.5                    | 451.2            | 0.795                                     | 277.1                             | $0.0047 \pm 0.0006$  | 273.6                                     | $0.0068 \pm 0.0020$  |
| 32.5                    | 447.8            | 0.797                                     | 278.6                             | $0.0036 \pm 0.0006$  | 277.3                                     | $0.0077 \pm 0.0020$  |
| 33.5                    | 449.0            | 0.795                                     | 280.6                             | $0.0045 \pm 0.0006$  | 273.8                                     | $0.0015 \pm 0.0019$  |
| 34.5                    | 445.9            | 0.787                                     | 281.2                             | $0.0059 \pm 0.0007$  | 277.1                                     | $0.0064 \pm 0.0020$  |
| 35.5                    | 451.3            | 0.790                                     | 281.1                             | $0.0036 \pm 0.0006$  | 275.1                                     | $0.0049 \pm 0.0021$  |
| 36.5                    | 448.8            | 0.785                                     | 281.3                             | $0.0044 \pm 0.0006$  | 272.1                                     | $0.0024 \pm 0.0019$  |
| 37.5                    | 451.6            | 0.784                                     | 282.8                             | $0.0039 \pm 0.0006$  | 271.3                                     | $0.0041 \pm 0.0019$  |
| 38.5                    | 453.3            | 0.779                                     | 284.2                             | $0.0046 \pm 0.0006$  | 268.3                                     | $0.0037 \pm 0.0019$  |
| 39.5                    | 452.9            | 0.790                                     | 284.8                             | $0.0039 \pm 0.0006$  | 270.9                                     | $0.0059 \pm 0.0019$  |
| $40.5 \\ 41.5$          | $456.0 \\ 452.7$ | $0.789 \\ 0.791$                          | 287.8<br>287.2                    | $0.0033 \pm 0.0006$<br>$0.0041 \pm 0.0006$   | $268.4 \\ 270.6$                          | $\begin{array}{c} 0.0027 \pm 0.0018 \\ 0.0057 \pm 0.0019 \end{array}$              |
| $41.5 \\ 42.5$          | 452.7 $453.2$    | 0.791                                     | 285.1                             | $0.0041 \pm 0.0006$<br>$0.0039 \pm 0.0006$   | 270.3                                     | $0.0037 \pm 0.0019$<br>$0.0067 \pm 0.0020$   |
| 43.5                    | 455.2            | 0.784                                     | 288.1                             | $0.0033 \pm 0.0000$<br>$0.0028 \pm 0.0005$   | 268.5                                     | $0.0057 \pm 0.0020$<br>$0.0057 \pm 0.0019$   |
| 44.5                    | 456.2            | 0.795                                     | 290.3                             | $0.0033 \pm 0.0005$  | 267.3                                     | $0.0045 \pm 0.0019$  |
| 45.5                    | 455.9            | 0.786                                     | 296.8                             | $0.0025 \pm 0.0005$  | 267.7                                     | $0.0041 \pm 0.0019$  |
| 46.5                    | 459.7            | 0.792                                     | 291.8                             | $0.0039 \pm 0.0005$  | 266.6                                     | $0.0076 \pm 0.0021$  |
| 47.5                    | 459.4            | 0.796                                     | 293.1                             | $0.0038 \pm 0.0006$  | 266.1                                     | $0.0022 \pm 0.0019$  |
| 48.5                    | 464.6            | 0.785                                     | 295.5                             | $0.0024 \pm 0.0005$  | 262.6                                     | $0.0041 \pm 0.0020$  |
| 49.5                    | 464.4            | 0.789                                     | 296.1                             | $0.0037 \pm 0.0005$  | 261.9                                     | $0.0070 \pm 0.0020$  |
| 50.5                    | 465.2            | 0.789                                     | 297.9                             | $0.0025 \pm 0.0005$  | 261.3                                     | $0.0016 \pm 0.0019$  |
| 51.5                    | 464.5            | 0.790                                     | 296.3                             | $0.0028 \pm 0.0005$  | 262.8                                     | $0.0070 \pm 0.0019$  |
| 52.5                    | 464.7            | 0.799                                     | 302.3                             | $0.0026 \pm 0.0005$  | 266.3                                     | $0.0054 \pm 0.0020$  |
| 53.5                    | 465.5            | 0.791                                     | 303.8                             | $0.0029 \pm 0.0005$  | 260.3                                     | $0.0049 \pm 0.0020$  |
| $54.5 \\ 55.5$          | $467.4 \\ 469.1$ | $0.789 \\ 0.790$                          | 301.5<br>305.7                    | $\begin{array}{c} 0.0030 \pm 0.0005 \\ 0.0021 \pm 0.0005 \end{array}$              | $262.0 \\ 261.5$                          | $\begin{array}{c} 0.0052 \pm 0.0020 \\ 0.0102 \pm 0.0022 \end{array}$              |
| 56.5                    | 470.0            | 0.790 $0.785$                             | 304.6                             | $0.0021 \pm 0.0005$<br>$0.0030 \pm 0.0005$   | 257.8                                     | $0.0102 \pm 0.0022$<br>$0.0059 \pm 0.0020$   |
| 57.5                    | 467.9            | 0.796                                     | 305.1                             | $0.0030 \pm 0.0005$<br>$0.0027 \pm 0.0005$   | 261.5                                     | $0.0059 \pm 0.0020$<br>$0.0050 \pm 0.0021$   |
| 58.5                    | 467.8            | 0.772                                     | 306.3                             | $0.0027 \pm 0.0005$<br>$0.0018 \pm 0.0005$   | 255.0                                     | $0.0050 \pm 0.0021$<br>$0.0057 \pm 0.0021$   |
| 59.5                    | 471.6            | 0.784                                     | 308.3                             | $0.0025 \pm 0.0005$  | 256.8                                     | $0.0047 \pm 0.0021$<br>$0.0047 \pm 0.0020$   |
| 60.5                    | 471.2            | 0.777                                     | 311.4                             | $0.0024 \pm 0.0005$  | 255.8                                     | $0.0038 \pm 0.0018$  |
| 61.5                    | 469.7            | 0.786                                     | 309.7                             | $0.0034 \pm 0.0005$  | 258.0                                     | $0.0054 \pm 0.0020$  |
| 62.5                    | 471.9            | 0.794                                     | 309.8                             | $0.0021 \pm 0.0005$  | 261.4                                     | $0.0039 \pm 0.0020$  |
| 63.5                    | 473.3            | 0.787                                     | 310.8                             | $0.0025 \pm 0.0005$  | 254.8                                     | $0.0073 \pm 0.0021$  |
| 64.5                    | 475.5            | 0.796                                     | 313.7                             | $0.0025 \pm 0.0005$  | 256.4                                     | $0.0053 \pm 0.0021$  |
| 65.5                    | 476.6            | 0.781                                     | 314.0                             | $0.0025 \pm 0.0005$  | 254.4                                     | $0.0031 \pm 0.0020$  |
| 66.5                    | 475.8            | 0.786                                     | 315.2                             | $0.0024 \pm 0.0005$  | 253.3                                     | $0.0068 \pm 0.0021$  |
| 67.5                    | 479.0            | 0.787                                     | 318.2                             | $0.0023 \pm 0.0005$  | 252.4                                     | $0.0085 \pm 0.0022$  |
| 68.5                    | 481.2            | 0.784                                     | 316.3                             | $0.0029 \pm 0.0005$  | 252.3                                     | $0.0049 \pm 0.0020$  |
| 69.5                    | 480.4            | 0.796                                     | 323.7                             | $0.0023 \pm 0.0005$  | 252.6                                     | $0.0069 \pm 0.0021$  |
| 70.5                    | 481.9            | 0.789                                     | 322.1                             | $0.0024 \pm 0.0005$  | 251.0                                     | $0.0031 \pm 0.0019$  |
| $71.5 \\ 72.5$          | 481.1            | 0.797                                     | 321.0                             | $\begin{array}{c} 0.0025 \pm 0.0005 \\ 0.0023 \pm 0.0005 \end{array}$              | 254.5                                     | $0.0046 \pm 0.0020$  |
| 73.5                    | 483.1 $487.3$    | 0.789 $0.784$                             | 320.6<br>319.9                    | $0.0023 \pm 0.0005$<br>$0.0023 \pm 0.0005$   | $249.5 \\ 249.1$                          | $\begin{array}{c} 0.0047 \pm 0.0019 \\ 0.0052 \pm 0.0020 \end{array}$              |
| $73.5 \\ 74.5$          | 485.8            | 0.784                                     | 326.4                             | $0.0023 \pm 0.0005$<br>$0.0028 \pm 0.0005$   | 249.1                                     | $0.0052 \pm 0.0020$<br>$0.0069 \pm 0.0021$   |
| 75.5                    | 485.2            | 0.787                                     | 324.2                             | $0.0028 \pm 0.0005$<br>$0.0024 \pm 0.0005$   | 252.5                                     | $0.0050 \pm 0.0021$<br>$0.0050 \pm 0.0020$   |
| 76.5                    | 488.8            | 0.783                                     | 327.9                             | $0.0024 \pm 0.0003$<br>$0.0020 \pm 0.0004$   | 246.8                                     | $0.0050 \pm 0.0020$<br>$0.0052 \pm 0.0019$   |
| 77.5                    | 488.6            | 0.798                                     | 321.1                             | $0.0017 \pm 0.0004$  | 251.0                                     | $0.0062 \pm 0.0010$<br>$0.0063 \pm 0.0020$   |
| 78.5                    | 489.2            | 0.788                                     | 330.2                             | $0.0030 \pm 0.0005$  | 245.7                                     | $0.0020 \pm 0.0019$  |
| 79.5                    | 486.1            | 0.787                                     | 328.7                             | $0.0019 \pm 0.0005$  | 245.9                                     | $0.0028 \pm 0.0018$  |
| 80.5                    | 490.4            | 0.793                                     | 333.5                             | $0.0023\pm0.0005$  | 247.2                                     | $0.0026 \pm 0.0019$  |

| 81.5  | 489.2 | 0.792 | 331.2 | $0.0018 \pm 0.0004$ | 247.6 | $0.0050 \pm 0.0021$  |
|-------|-------|-------|-------|---------------------|-------|----------------------|
| 82.5  | 491.4 | 0.789 | 329.4 | $0.0017 \pm 0.0004$ | 247.6 | $0.0058 \pm 0.0021$  |
| 83.5  | 490.0 | 0.790 | 328.8 | $0.0021 \pm 0.0005$ | 248.7 | $0.0056 \pm 0.0022$  |
| 84.5  | 488.1 | 0.790 | 328.9 | $0.0024 \pm 0.0005$ | 249.8 | $0.0081 \pm 0.0022$  |
| 85.5  | 492.4 | 0.798 | 331.8 | $0.0016 \pm 0.0005$ | 247.5 | $0.0055 \pm 0.0022$  |
| 86.5  | 493.1 | 0.778 | 332.3 | $0.0025 \pm 0.0005$ | 243.7 | $0.0025 \pm 0.0021$  |
| 87.5  | 493.9 | 0.790 | 332.4 | $0.0024 \pm 0.0005$ | 245.7 | $0.0046 \pm 0.0022$  |
| 88.5  | 494.7 | 0.790 | 337.3 | $0.0023 \pm 0.0005$ | 246.7 | $0.0034 \pm 0.0021$  |
| 89.5  | 498.1 | 0.796 | 332.7 | $0.0024 \pm 0.0005$ | 246.7 | $0.0043 \pm 0.0020$  |
| 90.5  | 498.2 | 0.794 | 335.5 | $0.0026 \pm 0.0005$ | 242.4 | $0.0052 \pm 0.0023$  |
| 91.5  | 498.1 | 0.783 | 331.8 | $0.0015 \pm 0.0005$ | 242.0 | $0.0049 \pm 0.0024$  |
| 92.5  | 496.2 | 0.796 | 336.1 | $0.0027 \pm 0.0005$ | 250.8 | $0.0007 \pm 0.0022$  |
| 93.5  | 497.2 | 0.786 | 335.3 | $0.0018 \pm 0.0005$ | 244.6 | $0.0054 \pm 0.0023$  |
| 94.5  | 498.5 | 0.782 | 337.2 | $0.0010 \pm 0.0005$ | 244.4 | $0.0070 \pm 0.0025$  |
| 95.5  | 501.0 | 0.793 | 336.6 | $0.0032 \pm 0.0006$ | 239.6 | $0.0009 \pm 0.0022$  |
| 96.5  | 500.0 | 0.798 | 336.8 | $0.0012 \pm 0.0005$ | 244.8 | $0.0012 \pm 0.0022$  |
| 97.5  | 498.8 | 0.783 | 335.6 | $0.0021 \pm 0.0006$ | 241.8 | $0.0043 \pm 0.0025$  |
| 98.5  | 503.9 | 0.799 | 341.0 | $0.0016 \pm 0.0006$ | 247.4 | $0.0064 \pm 0.0025$  |
| 99.5  | 499.6 | 0.803 | 336.5 | $0.0014 \pm 0.0005$ | 243.3 | $0.0020 \pm 0.0023$  |
| 100.5 | 499.1 | 0.788 | 340.3 | $0.0027 \pm 0.0006$ | 243.4 | $0.0012 \pm 0.0023$  |
| 101.5 | 502.4 | 0.803 | 338.7 | $0.0015 \pm 0.0006$ | 244.4 | $0.0060 \pm 0.0027$  |
| 102.5 | 502.7 | 0.787 | 339.9 | $0.0022 \pm 0.0006$ | 238.9 | $-0.0002 \pm 0.0026$ |
| 103.5 | 506.8 | 0.803 | 339.6 | $0.0025 \pm 0.0006$ | 239.3 | $0.0012 \pm 0.0025$  |
| 104.5 | 500.3 | 0.799 | 342.0 | $0.0021 \pm 0.0006$ | 242.2 | $0.0099 \pm 0.0033$  |
| 105.5 | 507.9 | 0.795 | 344.3 | $0.0031 \pm 0.0007$ | 238.8 | $-0.0025 \pm 0.0027$ |
| 106.5 | 504.4 | 0.787 | 338.7 | $0.0017 \pm 0.0006$ | 239.4 | $0.0022 \pm 0.0029$  |
| 107.5 | 509.0 | 0.780 | 342.3 | $0.0020 \pm 0.0007$ | 239.8 | $0.0026 \pm 0.0030$  |
| 108.5 | 505.8 | 0.766 | 338.8 | $0.0017 \pm 0.0007$ | 235.7 | $0.0025 \pm 0.0030$  |
| 109.5 | 508.9 | 0.794 | 343.4 | $0.0026 \pm 0.0007$ | 244.6 | $0.0057 \pm 0.0029$  |
| 110.5 | 510.0 | 0.791 | 347.3 | $0.0018 \pm 0.0007$ | 245.4 | $0.0034 \pm 0.0034$  |
| 111.5 | 510.0 | 0.791 | 345.7 | $0.0019 \pm 0.0007$ | 242.8 | $0.0058 \pm 0.0037$  |
| 112.5 | 510.0 | 0.817 | 345.8 | $0.0033 \pm 0.0009$ | 244.8 | $0.0007 \pm 0.0032$  |
| 113.5 | 510.0 | 0.798 | 346.4 | $0.0020 \pm 0.0009$ | 241.7 | $0.0109 \pm 0.0040$  |
| 114.5 | 510.0 | 0.797 | 346.5 | $0.0027 \pm 0.0009$ | 243.6 | $-0.0036 \pm 0.0032$ |
| 115.5 | 510.0 | 0.792 | 346.5 | $0.0021 \pm 0.0009$ | 239.3 | $0.0004 \pm 0.0033$  |
| 116.5 | 510.0 | 0.802 | 350.2 | $0.0010 \pm 0.0008$ | 245.0 | $0.0019 \pm 0.0036$  |
| 117.5 | 510.0 | 0.797 | 350.6 | $0.0023 \pm 0.0009$ | 242.5 | $0.0018 \pm 0.0040$  |
| 118.5 | 510.0 | 0.794 | 346.9 | $0.0027 \pm 0.0011$ | 247.0 | $0.0046 \pm 0.0043$  |
| 119.5 | 510.0 | 0.804 | 350.4 | $0.0008 \pm 0.0009$ | 236.8 | $0.0002 \pm 0.0036$  |
|       |       |       |       |                     |       |                      |

TABLE XXII: Measured cross sections for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=2.442$  GeV,  $|\theta_{pq}|=20.0^\circ,$  and  $E_{\rm miss}>25$  MeV. The  $P_{\rm miss}$  bins were 5 MeV/c wide. There is a 5.9% systematic uncertainty associated with these results.

| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
|--|---------------|------------|--------------------|--------------------|---------------------|---------|---------------------|
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$                   |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | $E_{ m miss}$ | $<\omega>$ |                    | $< P_{\rm miss} >$ |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | (MeV)         | (MeV)      | $(\text{GeV}/c)^2$ | (MeV/c)            | $(nb/MeV^2/sr^2)$   | (MeV/c) | $(nb/MeV^2/sr^2)$   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | 25.5          | 440.2      |                    | 339.4              | $0.0019 \pm 0.0003$ | 349.6   | $0.0002 \pm 0.0005$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | 26.5          | 439.3      | 0.790              | 340.7              | $0.0019 \pm 0.0003$ |         | $0.0011 \pm 0.0006$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | 27.5          | 441.4      | 0.796              | 346.8              | $0.0028 \pm 0.0003$ | 347.5   | $0.0015 \pm 0.0006$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | 28.5          | 441.7      | 0.792              |                    | $0.0012 \pm 0.0003$ | 347.6   | $0.0007 \pm 0.0005$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               | 440.0      |                    | 345.6              | $0.0018 \pm 0.0003$ | 346.9   | $0.0003 \pm 0.0004$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            | 0.792              |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | 36.5          |            | 0.785              |                    |                     | 340.3   |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    | —                   |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | 40.5          | 454.0      | 0.786              | 357.4              | $0.0016 \pm 0.0003$ | 335.4   | $0.0013 \pm 0.0005$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         | —                   |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         | —                   |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                    |               |            |                    |                    |                     |         |                     |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$                   |               |            |                    |                    | —                   |         | —                   |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$                   |               |            |                    |                    |                     |         |                     |
| 56.5 468.8 0.785 376.0 0.0021 $\pm$ 0.0003 325.6 0.0014 $\pm$ 0.0005     |               |            |                    |                    |                     |         |                     |
|  |               |            |                    |                    |                     |         | —                   |
| 57.5  472.0  0.788     374.1  0.0015 + 0.0003     324.8  0.0016 + 0.0007 |               |            |                    |                    |                     |         |                     |
| 5.15 1.215 5.165 5.111 5.0015 ± 6.0005 521.6 6.0016 ± 6.0001             | 57.5          | 472.0      | 0.788              | 374.1              | $0.0015 \pm 0.0003$ | 324.8   | $0.0016 \pm 0.0007$ |

| 58.5         471.2         0.779         375.0         0.0015 ± 0.0003         322.4         0.0016 ± 0.0006           60.5         472.9         0.784         377.0         0.0024 ± 0.0003         322.6         0.0020 ± 0.0007           61.5         472.3         0.792         378.6         0.0019 ± 0.0003         322.6         0.0020 ± 0.0007           62.5         473.6         0.789         377.8         0.0019 ± 0.0003         322.3         0.0011 ± 0.0007           63.5         475.0         0.785         381.2         0.0013 ± 0.0003         322.7         0.0019 ± 0.0006           65.5         478.8         0.789         385.5         0.0021 ± 0.0003         318.7         0.0020 ± 0.0007           66.5         478.8         0.780         382.1         0.013 ± 0.0003         317.9         0.0025 ± 0.0007           67.5         481.5         0.786         384.7         0.0022 ± 0.0003         317.9         0.0025 ± 0.0007           68.5         480.0         0.781         387.5         0.0022 ± 0.0003         317.9         0.0026 ± 0.0006           67.5         481.5         0.786         387.5         0.0012 ± 0.0006         316.8         0.0021 ± 0.0006           71.5         482.5  |       |       |       |       |                     |       |                      |
|--|-------|-------|-------|-------|---------------------|-------|----------------------|
| 60.5 472.9 0.784 377.0 0.0024 ± 0.0003 326.0 0.0024 ± 0.0007 62.5 473.6 0.789 377.8 0.0019 ± 0.0003 326.0 0.0024 ± 0.0007 62.5 473.6 0.789 377.8 0.0019 ± 0.0003 323.8 0.0011 ± 0.0007 63.5 475.0 0.785 381.2 0.0017 ± 0.0003 322.3 0.0015 ± 0.0007 65.5 478.8 0.789 385.5 0.0021 ± 0.0003 320.7 0.0019 ± 0.0006 65.5 478.8 0.799 385.1 0.0013 ± 0.0002 318.7 0.0022 ± 0.0007 66.5 478.8 0.799 382.1 0.0013 ± 0.0003 319.9 0.0015 ± 0.0006 67.5 481.5 0.786 384.7 0.0022 ± 0.0003 317.9 0.0025 ± 0.0007 67.5 481.5 0.786 384.7 0.0022 ± 0.0003 317.9 0.0025 ± 0.0007 67.5 481.5 0.786 384.7 0.0022 ± 0.0003 317.9 0.0025 ± 0.0007 67.5 481.3 0.788 387.5 0.0022 ± 0.0003 317.9 0.0026 ± 0.0008 69.5 480.3 0.788 387.5 0.0022 ± 0.0003 317.9 0.0026 ± 0.0008 69.5 480.3 0.788 387.5 0.0022 ± 0.0003 317.9 0.0026 ± 0.0008 69.5 480.3 0.788 387.5 0.0012 ± 0.0003 318.9 0.0024 ± 0.0006 71.5 481.3 0.786 387.5 0.0013 ± 0.0003 315.9 0.0024 ± 0.0007 73.5 486.6 0.791 393.4 0.0021 ± 0.0003 315.8 0.0022 ± 0.0007 73.5 486.6 0.791 393.4 0.0024 ± 0.0003 315.8 0.0022 ± 0.0007 73.5 486.6 0.791 393.4 0.0024 ± 0.0003 315.8 0.0025 ± 0.0007 76.5 485.3 0.792 394.3 0.0024 ± 0.0003 318.2 0.0018 ± 0.0007 76.5 485.0 0.787 393.7 0.0014 ± 0.0003 318.2 0.0018 ± 0.0007 76.5 485.0 0.787 393.7 0.0014 ± 0.0003 319.5 0.0012 ± 0.0007 78.5 486.0 0.798 396.0 0.0017 ± 0.0003 319.1 0.0022 ± 0.0008 82.5 494.0 0.801 399.2 0.0014 ± 0.0003 315.2 0.0006 ± 0.0008 82.5 494.0 0.801 399.2 0.0014 ± 0.0003 315.2 0.0006 ± 0.0008 82.5 494.0 0.801 399.2 0.0014 ± 0.0003 315.3 0.0022 ± 0.0008 82.5 494.0 0.801 399.2 0.0012 ± 0.0003 315.3 0.0022 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 315.3 0.0022 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 315.3 0.0022 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 310.4 0.0005 ± 0.0006 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 310.4 0.0002 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 310.4 0.0002 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 310.4 0.0002 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 310.4 0.0002 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0   | 58.5  | 471.2 | 0.779 | 375.0 | $0.0015 \pm 0.0003$ | 322.7 | $0.0018 \pm 0.0006$  |
| 61.5 472.3 0.792 378.6 0.0019 ± 0.0003 323.8 0.0011 ± 0.0007 63.5 475.0 0.791 380.8 0.0019 ± 0.0003 323.8 0.0011 ± 0.0007 63.5 475.0 0.785 381.2 0.0017 ± 0.0003 322.3 0.0015 ± 0.0007 64.5 476.0 0.785 381.2 0.0017 ± 0.0003 318.7 0.0029 ± 0.0006 65.5 478.8 0.789 385.5 0.0021 ± 0.0003 318.7 0.0022 ± 0.0007 66.5 478.8 0.789 385.1 0.0013 ± 0.0003 318.7 0.0025 ± 0.0006 66.5 478.8 0.789 385.1 0.0012 ± 0.0003 317.9 0.0025 ± 0.0006 68.5 480.0 0.791 387.0 0.0016 ± 0.0003 317.9 0.0025 ± 0.0006 68.5 480.0 0.791 387.0 0.0016 ± 0.0003 319.4 0.0014 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 317.9 0.0026 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 316.8 0.0024 ± 0.0006 71.5 480.9 0.782 383.3 0.0019 ± 0.0003 316.8 0.0024 ± 0.0006 72.5 482.5 0.792 394.3 0.0021 ± 0.0003 315.8 0.0025 ± 0.0007 72.5 482.5 0.792 394.3 0.0021 ± 0.0003 315.8 0.0025 ± 0.0007 72.5 482.5 0.792 394.3 0.0014 ± 0.0003 315.8 0.0025 ± 0.0007 74.5 486.2 0.781 395.4 0.0028 ± 0.0004 313.6 0.0012 ± 0.0006 75.5 485.3 0.792 393.4 0.0014 ± 0.0003 316.3 0.0021 ± 0.0006 75.5 485.3 0.792 393.4 0.0014 ± 0.0003 315.8 0.0021 ± 0.0006 75.5 485.3 0.792 393.4 0.0014 ± 0.0003 315.4 0.0012 ± 0.0006 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 315.4 0.0019 ± 0.0007 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 315.4 0.0019 ± 0.0007 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 315.4 0.0019 ± 0.0006 83.5 492.1 0.786 398.3 0.0023 ± 0.0003 312.8 0.0005 ± 0.0005 81.5 489.0 0.790 398.5 0.0018 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 398.9 0.0017 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 398.9 0.0017 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 402.1 0.0025 ± 0.0003 313.5 0.0028 ± 0.0008 83.5 492.1 0.786 402.5 0.0028 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 402.5 0.0028 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 402.5 0.0028 ± 0.0003 313.4 0.0004 ± 0.0007 9.5 504.6 0.798 401.9 0.0018 ± 0.0003 313.5 0.0028 ± 0.0008 83.5 492.1 0.786 402.5 0.0028 ± 0.0004 30.003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 31   | 59.5  | 471.4 | 0.779 | 376.5 | $0.0020 \pm 0.0003$ | 323.4 | $0.0016 \pm 0.0006$  |
| 61.5 472.3 0.792 378.6 0.0019 ± 0.0003 323.8 0.0011 ± 0.0007 63.5 475.0 0.791 380.8 0.0019 ± 0.0003 323.8 0.0011 ± 0.0007 63.5 475.0 0.785 381.2 0.0017 ± 0.0003 322.3 0.0015 ± 0.0007 64.5 476.0 0.785 381.2 0.0017 ± 0.0003 318.7 0.0029 ± 0.0006 65.5 478.8 0.789 385.5 0.0021 ± 0.0003 318.7 0.0022 ± 0.0007 66.5 478.8 0.789 385.1 0.0013 ± 0.0003 318.7 0.0025 ± 0.0006 66.5 478.8 0.789 385.1 0.0012 ± 0.0003 317.9 0.0025 ± 0.0006 68.5 480.0 0.791 387.0 0.0016 ± 0.0003 317.9 0.0025 ± 0.0006 68.5 480.0 0.791 387.0 0.0016 ± 0.0003 319.4 0.0014 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 317.9 0.0026 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 316.8 0.0024 ± 0.0006 71.5 480.9 0.782 383.3 0.0019 ± 0.0003 316.8 0.0024 ± 0.0006 72.5 482.5 0.792 394.3 0.0021 ± 0.0003 315.8 0.0025 ± 0.0007 72.5 482.5 0.792 394.3 0.0021 ± 0.0003 315.8 0.0025 ± 0.0007 72.5 482.5 0.792 394.3 0.0014 ± 0.0003 315.8 0.0025 ± 0.0007 74.5 486.2 0.781 395.4 0.0028 ± 0.0004 313.6 0.0012 ± 0.0006 75.5 485.3 0.792 393.4 0.0014 ± 0.0003 316.3 0.0021 ± 0.0006 75.5 485.3 0.792 393.4 0.0014 ± 0.0003 315.8 0.0021 ± 0.0006 75.5 485.3 0.792 393.4 0.0014 ± 0.0003 315.4 0.0012 ± 0.0006 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 315.4 0.0019 ± 0.0007 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 315.4 0.0019 ± 0.0007 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 315.4 0.0019 ± 0.0006 83.5 492.1 0.786 398.3 0.0023 ± 0.0003 312.8 0.0005 ± 0.0005 81.5 489.0 0.790 398.5 0.0018 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 398.9 0.0017 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 398.9 0.0017 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 402.1 0.0025 ± 0.0003 313.5 0.0028 ± 0.0008 83.5 492.1 0.786 402.5 0.0028 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 402.5 0.0028 ± 0.0003 313.5 0.0028 ± 0.0006 83.5 492.1 0.786 402.5 0.0028 ± 0.0003 313.4 0.0004 ± 0.0007 9.5 504.6 0.798 401.9 0.0018 ± 0.0003 313.5 0.0028 ± 0.0008 83.5 492.1 0.786 402.5 0.0028 ± 0.0004 30.003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 310.0003 31   | 60.5  | 472.9 | 0.784 | 377.0 |                     | 322.6 |                      |
| 62.5         473.6         0.789         377.8         0.0019 ± 0.0003         322.3         0.0011 ± 0.0007           63.5         476.0         0.785         381.2         0.0017 ± 0.0003         322.3         0.0019 ± 0.0006           65.5         478.8         0.789         385.5         0.0021 ± 0.0003         318.7         0.0025 ± 0.0007           67.5         481.5         0.786         384.7         0.0012 ± 0.0003         317.9         0.0025 ± 0.0007           68.5         480.0         0.791         387.0         0.0016 ± 0.0003         317.9         0.0025 ± 0.0007           69.5         480.3         0.788         387.5         0.0022 ± 0.0003         317.9         0.0026 ± 0.0008           70.5         480.9         0.782         383.3         0.0019 ± 0.0003         317.9         0.0026 ± 0.0008           71.5         481.3         0.786         387.5         0.0013 ± 0.0003         316.8         0.0024 ± 0.0007           72.5         482.5         0.792         394.3         0.0021 ± 0.0003         316.8         0.0022 ± 0.0007           73.5         486.6         0.791         393.4         0.0012 ± 0.0003         315.8         0.0012 ± 0.0007           74.5         487.0   |       | 472.3 |       |       |                     | 326.0 |                      |
| 63.5         475.0         0.791         380.8         0.0013 ± 0.0003         322.3         0.0015 ± 0.0007           64.5         476.0         0.785         381.2         0.0017 ± 0.0003         318.7         0.0020 ± 0.0007           66.5         478.8         0.789         385.5         0.0021 ± 0.0003         318.7         0.0025 ± 0.0007           66.5         480.0         0.791         387.0         0.0016 ± 0.0003         317.9         0.0025 ± 0.0007           68.5         480.0         0.782         383.3         0.0019 ± 0.0003         317.9         0.0026 ± 0.0008           70.5         480.9         0.782         383.3         0.0019 ± 0.0003         316.8         0.0024 ± 0.006           71.5         481.3         0.786         387.5         0.0013 ± 0.0003         316.8         0.0024 ± 0.006           71.5         481.3         0.786         387.5         0.0013 ± 0.0003         316.8         0.0024 ± 0.006           71.5         481.3         0.786         387.5         0.0013 ± 0.0003         315.8         0.0022 ± 0.006           72.5         482.5         0.792         393.4         0.0021 ± 0.0003         315.8         0.0022 ± 0.0007           74.5         485.0   |       |       |       |       |                     |       |                      |
| 64.5         476.0         0.785         381.2         0.0017 ± 0.0003         320.7         0.0019 ± 0.0006           66.5         478.8         0.790         382.1         0.0013 ± 0.0002         318.7         0.0022 ± 0.0007           67.5         481.5         0.786         384.7         0.0022 ± 0.0003         317.9         0.0025 ± 0.0007           69.5         480.0         0.791         387.0         0.0016 ± 0.0003         317.9         0.0025 ± 0.0004           69.5         480.3         0.788         387.5         0.0022 ± 0.0003         317.9         0.0026 ± 0.0004           71.5         481.3         0.786         387.5         0.0012 ± 0.0003         316.8         0.0024 ± 0.0007           71.5         481.3         0.786         387.5         0.0013 ± 0.0003         315.8         0.0022 ± 0.0007           72.5         482.5         0.792         394.3         0.0014 ± 0.0003         316.3         0.0021 ± 0.0007           73.5         486.6         0.791         393.4         0.0014 ± 0.0003         316.3         0.0021 ± 0.0007           74.5         486.2         0.781         393.7         0.0014 ± 0.0003         316.4         0.0019 ± 0.0007           75.5         485.3   |       |       |       |       |                     |       |                      |
| 65.5 478.8 0.789 385.5 0.0021 ± 0.0003 318.7 0.0020 ± 0.0006 67.5 478.8 0.790 382.1 0.0013 ± 0.0003 319.9 0.0015 ± 0.0006 67.5 481.5 0.786 384.7 0.0022 ± 0.0003 317.9 0.0025 ± 0.0007 68.5 480.0 0.791 387.0 0.0016 ± 0.0003 317.9 0.0026 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 317.9 0.0026 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 316.8 0.0024 ± 0.0006 71.5 481.3 0.786 387.5 0.0012 ± 0.0003 316.8 0.0024 ± 0.0006 72.5 482.5 0.792 394.3 0.0021 ± 0.0003 315.8 0.0022 ± 0.0007 72.5 482.5 0.792 394.3 0.0021 ± 0.0003 315.8 0.0021 ± 0.0007 74.5 486.6 0.791 393.4 0.0014 ± 0.0003 316.3 0.0021 ± 0.0007 74.5 486.5 0.781 393.4 0.0014 ± 0.0003 318.2 0.0012 ± 0.0007 74.5 486.5 0.781 393.4 0.0014 ± 0.0003 318.2 0.0012 ± 0.0006 75.5 485.3 0.792 393.4 0.0014 ± 0.0003 318.2 0.0018 ± 0.0007 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 319.1 0.0022 ± 0.0006 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 319.1 0.0022 ± 0.0008 79.5 488.3 0.785 398.3 0.0023 ± 0.0003 319.1 0.0022 ± 0.0008 81.5 488.4 0.801 396.4 0.0019 ± 0.0003 315.2 0.0016 ± 0.0005 81.5 489.0 0.790 398.5 0.0018 ± 0.0003 315.3 0.0022 ± 0.0008 82.5 494.0 0.801 399.2 0.0018 ± 0.0003 315.3 0.0022 ± 0.0008 83.5 499.1 0.786 398.9 0.0017 ± 0.0003 313.5 0.0022 ± 0.0008 83.5 499.1 0.786 398.9 0.0017 ± 0.0003 313.3 0.0024 ± 0.0008 83.5 499.1 0.786 398.9 0.0017 ± 0.0003 313.3 0.0024 ± 0.0008 83.5 499.1 0.786 402.1 0.0015 ± 0.0003 313.4 0.0002 ± 0.0008 83.5 499.1 0.786 402.3 0.0018 ± 0.0003 313.4 0.0002 ± 0.0008 83.5 499.1 0.786 402.3 0.0018 ± 0.0003 313.4 0.0002 ± 0.0008 83.5 501.1 0.805 402.1 0.0015 ± 0.0003 313.4 0.0002 ± 0.0008 83.5 501.1 0.805 402.1 0.0015 ± 0.0003 313.4 0.0002 ± 0.0008 83.5 501.1 0.805 402.1 0.0015 ± 0.0003 313.0 0.0013 ± 0.0009 91.5 497.4 0.789 402.5 0.0022 ± 0.0003 313.0 0.0013 ± 0.0009 91.5 497.4 0.789 402.5 0.0022 ± 0.0003 306.8 0.0025 ± 0.0008 89.5 503.8 0.797 407.5 0.0018 ± 0.0004 309.5 0.0018 ± 0.0005 30.8 0.0022 ± 0.0008 91.5 503.8 0.799 402.5 0.0022 ± 0.0003 306.8 0.0022 ± 0.0008 91.5 503.8 0.799 402.5 0.0022 ± 0.0004 309.5 0.0018 ± 0.0009 30.5 503.8 0   |       |       |       |       | —                   |       | —                    |
| 66.5 478.8 0.790   |       |       |       |       |                     |       |                      |
| 68.5 481.5 0.786 384.7 0.0022 ± 0.0003 317.9 0.0025 ± 0.0007 68.5 480.0 0.791 387.0 0.0016 ± 0.0003 317.9 0.0026 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 317.9 0.0026 ± 0.0008 70.5 480.9 0.782 383.3 0.0019 ± 0.0003 316.8 0.0024 ± 0.0006 71.5 481.3 0.786 387.5 0.0013 ± 0.0003 317.9 0.0026 ± 0.0007 72.5 482.5 0.792 394.3 0.0014 ± 0.0003 315.8 0.0025 ± 0.0007 72.5 482.5 0.792 394.3 0.0014 ± 0.0003 315.8 0.0025 ± 0.0007 74.5 486.6 0.791 393.4 0.0014 ± 0.0003 316.3 0.0021 ± 0.0007 74.5 486.6 0.791 393.4 0.0014 ± 0.0003 316.3 0.0021 ± 0.0007 74.5 486.6 0.791 393.4 0.0014 ± 0.0003 318.2 0.0018 ± 0.0007 77.5 487.0 0.798 393.4 0.0014 ± 0.0003 318.2 0.0018 ± 0.0007 77.5 487.0 0.798 396.2 0.0014 ± 0.0003 319.1 0.0022 ± 0.0008 78.5 488.3 0.785 398.3 0.0021 ± 0.0003 319.1 0.0022 ± 0.0008 79.5 488.3 0.785 398.3 0.0023 ± 0.0003 312.8 0.0005 ± 0.0005 80.5 488.4 0.801 396.4 0.0019 ± 0.0003 315.2 0.0006 ± 0.0005 81.5 489.0 0.790 398.5 0.0018 ± 0.0003 315.3 0.0022 ± 0.0008 82.5 494.0 0.801 396.2 0.0018 ± 0.0003 315.3 0.0022 ± 0.0008 82.5 494.0 0.801 399.2 0.0012 ± 0.0003 315.3 0.0022 ± 0.0008 83.5 499.1 0.786 398.9 0.0017 ± 0.0003 313.3 0.0022 ± 0.0008 84.5 493.7 0.791 400.6 0.0022 ± 0.0003 313.3 0.0022 ± 0.0008 85.5 496.6 0.798 400.1 0.0025 ± 0.0003 313.3 0.0024 ± 0.0008 86.5 496.6 0.798 400.1 0.0025 ± 0.0003 313.4 0.0004 ± 0.0007 9.006 86.5 496.6 0.798 400.1 0.0025 ± 0.0003 313.4 0.0004 ± 0.0007 9.05 400.5 402.1 0.0003 313.5 0.0023 ± 0.0008 88.5 499.0 0.799 401.4 0.0015 ± 0.0003 306.8 0.0023 ± 0.0008 88.5 500.1 0.789 402.5 0.0002 ± 0.0003 306.8 0.0023 ± 0.0008 88.5 500.1 0.789 402.5 0.0002 ± 0.0003 306.8 0.0023 ± 0.0008 88.5 500.1 0.789 402.5 0.0002 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.0003 306.8 0.0025 ± 0.   |       |       |       |       |                     |       |                      |
| 68.5         480.0         0.791         387.0         0.0016 ± 0.0003         319.4         0.0014 ± 0.0006           70.5         480.9         0.782         383.3         0.0019 ± 0.0003         316.8         0.0024 ± 0.0006           71.5         481.3         0.786         387.5         0.0013 ± 0.0003         319.5         0.0012 ± 0.0007           72.5         482.5         0.792         394.3         0.0021 ± 0.0003         315.8         0.0022 ± 0.0007           73.5         486.6         0.781         393.4         0.0014 ± 0.0003         316.3         0.0021 ± 0.0007           74.5         486.2         0.781         393.4         0.0014 ± 0.0003         318.2         0.0018 ± 0.0007           75.5         485.3         0.792         393.4         0.0014 ± 0.0003         318.2         0.0018 ± 0.0007           76.5         485.0         0.787         393.7         0.0014 ± 0.0003         318.1         0.0019 ± 0.0007           78.5         486.4         0.788         396.0         0.0017 ± 0.0003         319.1         0.0022 ± 0.0008           78.5         488.4         0.801         396.4         0.0019 ± 0.0003         315.2         0.0066 ± 0.0055           80.5         489.0   |       |       |       |       |                     |       |                      |
| 69.5         480.3         0.782         383.3         0.0019 ± 0.0003         317.9         0.0026 ± 0.0006           70.5         480.9         0.782         383.3         0.0019 ± 0.0003         316.8         0.0024 ± 0.0006           71.5         481.3         0.786         387.5         0.0013 ± 0.0003         315.8         0.0025 ± 0.0007           73.5         486.6         0.791         393.4         0.0014 ± 0.0003         316.3         0.0012 ± 0.0007           74.5         486.2         0.781         395.4         0.0028 ± 0.0004         313.6         0.0012 ± 0.0007           75.5         485.0         0.787         393.7         0.0014 ± 0.0003         318.2         0.0018 ± 0.0007           76.5         485.0         0.788         396.2         0.0014 ± 0.0003         319.1         0.0022 ± 0.0008           79.5         488.3         0.785         398.3         0.0017 ± 0.0003         312.8         0.0018 ± 0.0007           77.5         487.0         0.788         396.2         0.0014 ± 0.0003         315.2         0.0018 ± 0.0008           79.5         488.3         0.785         398.3         0.0023 ± 0.0003         315.2         0.0006 ± 0.0005           81.5         489.0   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
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| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 81.5  | 489.0 | 0.790 | 398.5 |                     | 313.5 |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       | 494.0 | 0.801 | 399.2 |                     | 315.3 |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       | 0.786 |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 84.5  |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 85.5  | 495.2 | 0.798 | 400.1 | $0.0025 \pm 0.0003$ | 313.6 | $0.0023 \pm 0.0008$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 86.5  | 496.6 | 0.798 | 401.9 | $0.0018 \pm 0.0003$ | 310.4 | $0.0007 \pm 0.0006$  |
| $\begin{array}{c} 89.5  500.1  0.789 \\ 90.5  496.2  0.796 \\ 91.5  497.4  0.789 \\ 92.5  497.4  0.789 \\ 92.5  497.1  0.789 \\ 93.5  499.7  0.780 \\ 94.5  500.9  0.789 \\ 96.5  502.5  0.797 \\ 407.1  0.0019 \pm 0.0003 \\ 96.5  502.5  0.797 \\ 407.1  0.0019 \pm 0.0003 \\ 96.5  502.5  0.786 \\ 407.1  0.0019 \pm 0.0003 \\ 90.5  500.9  0.789 \\ 96.5  502.5  0.797 \\ 407.1  0.0015 \pm 0.0004 \\ 96.5  502.5  0.797 \\ 407.1  0.0015 \pm 0.0004 \\ 407.3  0.0015 \pm 0.0004 \\ 408.5  500.9  0.780 \\ 96.5  502.5  0.797 \\ 407.1  0.0021 \pm 0.0004 \\ 97.5  501.8  0.786 \\ 407.3  0.0015 \pm 0.0004 \\ 407.4  0.0015 \pm 0.0004 \\ 407.5  0.0019 \pm 0.0004 \\ 408.5  503.8  0.790 \\ 407.4  0.0015 \pm 0.0004 \\ 407.4  0.0015 \pm 0.0003 \\ 407.4  0.0015 \pm 0.0003 \\ 407.4  0.0015 \pm 0.0003 \\ 407.5  0.0019 \pm 0.0004 \\ 407.5  0.0016 \pm 0.0004 \\ 407.7  0.0010 \pm 0.0003 \\ 407.7  0.0010 \pm 0.0004 \\ 407.7  0.0010 \pm 0.0004 \\ 407.7  0.0010 \pm 0.0005 \\ 407.7  $ | 87.5  | 501.1 | 0.805 | 402.1 | $0.0015 \pm 0.0003$ | 311.9 | $0.0019 \pm 0.0008$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 88.5  | 499.0 | 0.790 | 401.4 | $0.0015 \pm 0.0003$ | 306.8 | $0.0025 \pm 0.0008$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 89.5  | 500.1 | 0.789 | 402.5 | $0.0020 \pm 0.0003$ | 306.3 | $0.0013 \pm 0.0007$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 90.5  | 496.2 | 0.796 | 402.3 | $0.0018 \pm 0.0003$ | 311.2 | $0.0021 \pm 0.0009$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 91.5  | 497.4 | 0.789 | 404.9 | $0.0019 \pm 0.0003$ | 308.8 | $0.0030 \pm 0.0009$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 92.5  | 497.1 | 0.799 | 402.5 | $0.0022 \pm 0.0003$ | 313.8 | $0.0006 \pm 0.0009$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 93.5  | 499.7 | 0.780 | 404.7 | $0.0015 \pm 0.0003$ | 307.9 | $0.0023 \pm 0.0009$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 94.5  | 500.9 | 0.789 | 409.6 | $0.0018 \pm 0.0004$ | 307.4 | $0.0032 \pm 0.0008$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 95.5  | 503.8 | 0.797 | 407.5 | $0.0019 \pm 0.0004$ | 306.9 | $-0.0001 \pm 0.0006$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 96.5  | 502.5 | 0.797 | 407.1 | $0.0021 \pm 0.0004$ | 309.5 | $0.0013 \pm 0.0007$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 97.5  | 501.8 | 0.786 | 407.3 | $0.0015 \pm 0.0004$ | 306.1 | $0.0026 \pm 0.0008$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 98.5  | 503.8 | 0.790 | 405.6 | $0.0018 \pm 0.0004$ | 311.0 | $-0.0007 \pm 0.0007$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 99.5  | 504.3 | 0.794 | 407.4 | $0.0015 \pm 0.0003$ | 308.6 | $0.0042 \pm 0.0011$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 100.5 |       | 0.797 | 406.2 | $0.0016 \pm 0.0004$ | 309.0 | $0.0018 \pm 0.0010$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 101.5 | 505.3 | 0.790 | 409.4 | $0.0010 \pm 0.0003$ | 306.1 | $0.0023 \pm 0.0010$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 102.5 | 503.3 | 0.801 | 408.5 | $0.0020 \pm 0.0004$ | 310.8 | $0.0003 \pm 0.0009$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 103.5 | 506.0 | 0.796 | 407.7 | $0.0010 \pm 0.0004$ | 310.1 | $0.0027 \pm 0.0009$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 104.5 | 507.6 |       |       |                     | 305.8 |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 105.5 | 506.7 | 0.788 | 411.3 | $0.0023 \pm 0.0005$ | 304.2 | $0.0016 \pm 0.0011$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 106.5 | 508.3 | 0.802 | 414.0 | $0.0018 \pm 0.0004$ | 306.7 | $0.0029 \pm 0.0011$  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 107.5 | 511.2 | 0.807 | 411.2 |                     | 309.6 |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 109.5 | 508.6 | 0.786 | 412.4 |                     | 308.9 |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |       |       |       |                     |       |                      |
| 118.5 515.0 0.771 415.4 $0.0004 \pm 0.0006$ 300.5 $0.0014 \pm 0.0017$  |       |       |       |       |                     |       |                      |
|  |       |       |       |       |                     |       |                      |
|  |       |       |       |       |                     |       |                      |

## 2. Asymmetries and response functions

## $a. \quad 1p\text{-}shell$

Response functions and asymmetries for QE proton knockout from  $^{16}{\rm O}$  are presented in Tables XXIII, XXIV, and XXV.

TABLE XXIII: Separated response functions  $R_L$  and  $R_T$  for QE proton knockout from the 1p-shell of  $^{16}{\rm O}$  for  $< T_p > = 427$  MeV. The  $P_{\rm miss}$  bins were 20 MeV/c wide. Cuts were applied to remove the radiative tail from  $^{1}{\rm H}(e,ep)$  such that  $< P_{\rm miss} > = 52.5$  MeV/c in each case. Note that the  $\omega$  acceptance of the three measurements was shifted by about 3% in order to keep the phase-space acceptance flat. The resulting change in the domain was taken as an additional 4% systematic uncertainty.

|                                |                          | $1p_{1/2}$ -state        |                    |                          | $1p_{3/2}$ -state        |
|--------------------------------|--------------------------|--------------------------|--------------------|--------------------------|--------------------------|
| $\langle P_{\rm miss} \rangle$ | $R_L / \text{fm}^3$      | $R_T / \text{fm}^3$      | $< P_{\rm miss} >$ | $R_L / \text{fm}^3$      | $R_T / \text{fm}^3$      |
| (MeV/c)                        | (stat) (sys)             | (stat) (sys)             | (MeV/c)            | (stat) (sys)             | (stat) (sys)             |
| 52.5                           | $1.82 \pm 1.17 \pm 0.59$ | $7.58 \pm 1.42 \pm 0.72$ | 52.5               | $2.35 \pm 1.18 \pm 0.73$ | $9.40 \pm 1.39 \pm 0.85$ |

TABLE XXIV: Separated response functions  $R_{L+TT}$  and  $R_T$  for QE proton knockout from the 1p-shell of  $^{16}{\rm O}$  for  $< Q^2>=0.800~({\rm GeV/c})^2, <\omega>=436~{\rm MeV},$  and  $< T_p>=427~{\rm MeV}$ . The  $P_{\rm miss}$  bins were 20 MeV/c wide.

|                    |                              | $1p_{1/2}$ -state        |                    |                              | $1p_{3/2}$ -state         |
|--------------------|------------------------------|--------------------------|--------------------|------------------------------|---------------------------|
| $< P_{\rm miss} >$ | $R_{L+TT}$ / fm <sup>3</sup> | $R_T / \text{fm}^3$      | $< P_{\rm miss} >$ | $R_{L+TT}$ / fm <sup>3</sup> | $R_T / \text{fm}^3$       |
| (MeV/c)            | (stat) (sys)                 | (stat) (sys)             | (MeV/c)            | (stat) (sys)                 | (stat) (sys)              |
| 149.0              | $0.56 \pm 0.49 \pm 0.12$     | $6.08 \pm 0.61 \pm 0.24$ | 149.0              | $2.20 \pm 0.75 \pm 0.30$     | $10.35 \pm 1.04 \pm 0.43$ |
| 279.0              | $0.01\pm0.03\pm0.01$         | $0.12 \pm 0.04 \pm 0.01$ | 276.0              | $0.20\pm0.06\pm0.03$         | $0.29 \pm 0.08 \pm 0.01$  |

TABLE XXV: Separated asymmetries  $A_{LT}$  and response functions  $R_{LT}$  for QE proton knockout from the 1p-shell of  $^{16}{\rm O}$  for  $< Q^2>=0.800~({\rm GeV}/c)^2, <\omega>=436~{\rm MeV},$  and  $< T_p>=427~{\rm MeV}$ . The  $P_{\rm miss}$  bins were 20 MeV/c wide. Save for the data labelled [\*] which were obtained at  $E_{\rm beam}=1.643~{\rm GeV},$  the beam energy was 2.442 GeV.

|                    |                           | $1p_{1/2}$ -state            |                    |                           | $1p_{3/2}$ -state            |
|--------------------|---------------------------|------------------------------|--------------------|---------------------------|------------------------------|
| $< P_{\rm miss} >$ | $A_{LT}$ /                | $R_{LT}$ / fm <sup>3</sup>   | $< P_{\rm miss} >$ | $A_{LT}$ /                | $R_{LT}$ / fm <sup>3</sup>   |
| (MeV/c)            | (stat) (sys)              | (stat) (sys)                 | (MeV/c)            | (stat) (sys)              | (stat) (sys)                 |
| 60.0               |                           | $0.117 \pm 0.134 \pm 0.037$  |                    |                           | $-0.754 \pm 0.165 \pm 0.084$ |
| 148.0 [*]          | $-0.25 \pm 0.02 \pm 0.03$ | $-1.198 \pm 0.235 \pm 0.085$ | 147.0 [*]          | $-0.31 \pm 0.04 \pm 0.03$ | $-2.820 \pm 0.292 \pm 0.183$ |
| 149.0              | $-0.23 \pm 0.02 \pm 0.03$ | $-0.999 \pm 0.066 \pm 0.077$ | 148.0              | $-0.31 \pm 0.01 \pm 0.03$ | $-2.560 \pm 0.096 \pm 0.173$ |
| 279.0              | $-0.36 \pm 0.08 \pm 0.04$ | $-0.029 \pm 0.007 \pm 0.002$ | 276.0              | $-0.69 \pm 0.04 \pm 0.04$ | $-0.250 \pm 0.013 \pm 0.019$ |
| 345.0              | $-0.13 \pm 0.22 \pm 0.05$ | $-0.002 \pm 0.003 \pm 0.001$ | 345.0              | $-0.39 \pm 0.08 \pm 0.05$ | $-0.015 \pm 0.003 \pm 0.001$ |

## b. Higher missing energies

Response functions for QE proton knockout from  $^{16}{\rm O}$  for  $E_{\rm miss}>25$  MeV are presented in Tables XXVI through XXVIII.

TABLE XXVI: Separated response functions  $R_L$  and  $R_T$  for QE proton knockout from  $^{16}{\rm O}$  at  $\theta_{pq}=0^{\circ}$  for  $E_{\rm miss}>25$  MeV. The  $E_{\rm miss}$  bins are 5 MeV wide.

| $\langle E_{\rm miss} \rangle$ | $R_L / \text{fm}^3/\text{MeV}$  | $R_T / \text{fm}^3/\text{MeV}$ |
|--------------------------------|---------------------------------|--------------------------------|
| (MeV)                          | ()                              |                                |
| 27.5                           |                                 |                                |
| 32.5                           |                                 |                                |
| 37.5                           | $0.141 \pm 0.040 \pm 0.052$     | $0.523 \pm 0.049 \pm 0.051$    |
| 42.5                           | $0.138 \pm 0.037 \pm 0.063$     | $0.600 \pm 0.044 \pm 0.066$    |
| 47.5                           | $0.100 \pm 0.039 \pm 0.054$     | $0.517 \pm 0.047 \pm 0.051$    |
| 52.5                           | $0.054 \pm 0.044 \pm 0.049$     | $0.304 \pm 0.054 \pm 0.028$    |
| 57.5                           | $\text{-0.047}\pm0.111\pm0.030$ | $0.253 \pm 0.145 \pm 0.049$    |

TABLE XXVII: Separated response functions  $R_{L+TT}$  and  $R_T$  for QE proton knockout from  $^{16}{\rm O}$  at  $\theta_{pq}=8^{\circ}$  and  $\theta_{pq}=16^{\circ}$  for  $E_{\rm miss}>25$  MeV. The  $E_{\rm miss}$  bins are 5 MeV wide.

|                                |                                   | $\theta_{pq}=8^{\circ}$        |                                   | $\theta_{pq}=16^{\circ}$       |
|--------------------------------|-----------------------------------|--------------------------------|-----------------------------------|--------------------------------|
| $\langle E_{\rm miss} \rangle$ | $R_{L+TT}$ / fm <sup>3</sup> /MeV | $R_T / \text{fm}^3/\text{MeV}$ | $R_{L+TT}$ / fm <sup>3</sup> /MeV | $R_T / \text{fm}^3/\text{MeV}$ |
| (MeV)                          | (stat) (sys)                      | (stat) (sys)                   | (stat) (sys)                      | (stat) (sys)                   |
| 27.5                           | $0.080 \pm 0.023 \pm 0.010$       | $0.137 \pm 0.029 \pm 0.008$    | $0.002 \pm 0.004 \pm 0.003$       | $0.027 \pm 0.005 \pm 0.005$    |
| 32.5                           | $0.072 \pm 0.021 \pm 0.008$       | $0.133 \pm 0.026 \pm 0.008$    | $-0.001 \pm 0.004 \pm 0.001$      | $0.026 \pm 0.005 \pm 0.001$    |
| 37.5                           | $0.075 \pm 0.021 \pm 0.008$       | $0.162 \pm 0.027 \pm 0.010$    | $0.001 \pm 0.004 \pm 0.001$       | $0.018 \pm 0.004 \pm 0.001$    |
| 42.5                           | $0.087 \pm 0.021 \pm 0.013$       | $0.164 \pm 0.026 \pm 0.010$    | $0.005 \pm 0.004 \pm 0.001$       | $0.014 \pm 0.004 \pm 0.001$    |
| 47.5                           | $0.050 \pm 0.022 \pm 0.008$       | $0.172 \pm 0.028 \pm 0.010$    | $0.001 \pm 0.004 \pm 0.001$       | $0.017 \pm 0.005 \pm 0.001$    |
| 52.5                           | $0.001 \pm 0.022 \pm 0.006$       | $0.137 \pm 0.027 \pm 0.009$    | $0.005 \pm 0.005 \pm 0.001$       | $0.018 \pm 0.006 \pm 0.002$    |
| 57.5                           | $\text{-0.002}\pm0.024\pm0.004$   | $0.010 \pm 0.030 \pm 0.006$    | $0.008 \pm 0.007 \pm 0.001$       | $0.008 \pm 0.007 \pm 0.001$    |

TABLE XXVIII: Separated asymmetries  $A_{LT}$  and response functions  $R_{LT}$  for QE proton knockout from  $^{16}{\rm O}$  for at  $\theta_{pq}=8^{\circ}$  and  $\theta_{pq}=16^{\circ}$  for  $E_{\rm miss}>25$  MeV. The  $E_{\rm miss}$  bins are 5 MeV wide. Note that the data presented for  $\theta_{pq}=8^{\circ}$  represent the average of the data obtained at  $E_{\rm beam}=1.643$  GeV and  $E_{\rm beam}=2.442$  GeV.

|                    | $\theta_{pq}=8^{\circ}$           | $\theta_{pq} = 16^{\circ}$        |
|--------------------|-----------------------------------|-----------------------------------|
| $< E_{\rm miss} >$ | $R_{LT} / \text{fm}^3/\text{MeV}$ | $R_{LT} / \text{fm}^3/\text{MeV}$ |
| (MeV)              | (stat) (sys)                      |                                   |
|                    | $-0.070 \pm 0.006 \pm 0.005$      |                                   |
|                    | $-0.050 \pm 0.005 \pm 0.004$      |                                   |
| 37.5               | $-0.076 \pm 0.005 \pm 0.010$      | $-0.007 \pm 0.001 \pm 0.002$      |
|                    | $-0.083 \pm 0.006 \pm 0.039$      |                                   |
| 47.5               | $-0.077 \pm 0.006 \pm 0.010$      | $-0.004 \pm 0.002 \pm 0.001$      |
| 52.5               | $-0.036 \pm 0.006 \pm 0.015$      | $-0.004 \pm 0.002 \pm 0.001$      |
| 57.5               | $-0.036 \pm 0.006 \pm 0.005$      | $-0.004 \pm 0.003 \pm 0.001$      |

# APPENDIX B: THE DIP-REGION INVESTIGATION

A small portion of the beam time allocated to the measurement discussed in the main body of this article was used for an exploratory investigation of the "dip" region located in the energy transfer domain between the QE peak and the  $\Delta(1232)$ -resonance. For this investigation,  $E_{\text{beam}} = 1.643 \text{ GeV}$  was employed, and the HRS<sub>e</sub> position and central momentum were fixed at  $\theta_e = 37.17^{\circ}$ and  $p_e = 1056 \text{ MeV}/c$ , respectively. This resulted in  $|\vec{q}|$  $\approx 1.026 \text{ GeV}/c$ ,  $\omega \approx 589 \text{ MeV}$ , and  $Q^2 = 0.706 \text{ (GeV}/c)^2$ [137]. The HRS<sub>h</sub> was then positioned at  $\theta_h = 38.45^{\circ}$  $(\theta_{pq} = 0^{\circ})$  and its central momentum varied from 828 MeV/c to 1190 MeV/c in five steps of  $\Delta p_p \approx 70 \text{ MeV}/c$ per step. These momentum settings were close enough to each other that there was adequate acceptance overlap between them to allow for radiative corrections to be performed. The configuration of the experimental apparatus and data acquisition system was identical in all aspects to that used for the QE measurement. The data analysis was also identical to that performed on the QE data, save for an additional cut to remove contamination from  $H(e, e'p)\pi^0$  events.

Figure 26 shows the measured cross sections for the dip region as a function of  $E_{\rm miss}$  compared to calculations by the Ghent Group for  $E_{\rm beam}=1.643$  GeV (see Table XXIX). The error bars are statistical. There is on average an additional 5.8% systematic uncertainty (see Table XXIX) associated with the data. The dashed curve is the "bare" ROMEA calculation for proton knockout from the  $1s_{1/2}$ -state of  $^{16}{\rm O}$  and the solid curve is the same calculation including the effects of MEC and IC (see the main text of this article for further details). The normalization factor of 1.00 employed for these calculations was that which the best results for the QE data. The dashed-dotted curve illustrates the incoherent sum of the "full" calculation and the computed (e,e'pn) and (e,e'pp) contribution.

In contrast to the QE energy domain, the "bare" calculation actually overestimated the  $1s_{1/2}$ -state strength in these kinematics. Also in contrast to the QE energy domain, the inclusion of MEC and IC decrease the magnitude of the calculated cross sections and improve the agreement. Finally, while the (e,e'pX) calculations have the measured flat shape for  $E_{\rm miss}>100$  MeV, they are twice as large as the cross sections.

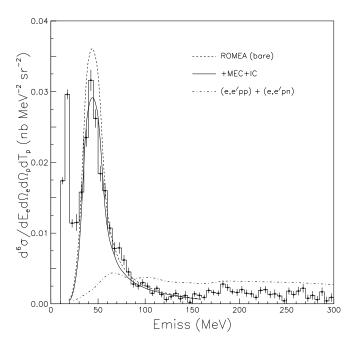


FIG. 26: Data from this work together with calculations by the Ghent Group for the  $E_{\rm miss}$ -dependence of the cross sections obtained in dip-region kinematics for  $E_{\rm beam}=1.643$  GeV. Error bars are statistical and on average, there is an additional  $\pm 5.9\%$  systematic uncertainty (see Table XXIX) associated with the data.

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TABLE XXIX: Measured cross sections for proton knockout from  $^{16}{\rm O}$  for  $E_{\rm beam}=1.643~{\rm GeV}$  in dip-region kinematics for  $E_{\rm miss}>25~{\rm MeV}.$  The  $E_{\rm miss}$  bins were 5 MeV wide. There is a 5.9% systematic uncertainty associated with these results.

| $E_{ m miss}$ | $< P_{ m miss} >$ | $d^6\sigma/d\omega dE_p d\Omega_e d\Omega_p$ |
|---------------|-------------------|--|
| (MeV)         | (MeV)             | $(\text{nb/MeV}^2/\text{sr}^2)$              |
| /             | ( /               |  |
| 27.5          | 163.6             | $0.0115 \pm 0.0012$                          |
| 32.5          | 152.1             | $0.0158 \pm 0.0012$                          |
| 37.5          | 138.8             | $0.0235 \pm 0.0013$                          |
| 42.5          | 132.8             | $0.0316 \pm 0.0015$                          |
| 47.5          | 128.3             | $0.0262 \pm 0.0013$                          |
| 52.5          | 119.4             | $0.0184 \pm 0.0011$                          |
| 57.5          | 112.1             | $0.0160 \pm 0.0011$                          |
| 62.5          | 107.5             | $0.0107 \pm 0.0009$                          |
|               |                   |  |
| 67.5          | 95.0              | $0.0078 \pm 0.0009$                          |
| 72.5          | 95.0              | $0.0079 \pm 0.0008$                          |
| 77.5          | 95.0              | $0.0062 \pm 0.0007$                          |
| 82.5          | 90.0              | $0.0045 \pm 0.0006$                          |
| 87.5          | 84.0              | $0.0028 \pm 0.0005$                          |
| 92.5          | 76.0              | $0.0025 \pm 0.0005$                          |
| 97.5          | 71.7              | $0.0030 \pm 0.0005$                          |
| 102.5         | 68.0              | $0.0025 \pm 0.0005$                          |
| 107.5         | 60.0              | $0.0025 \pm 0.0005$<br>$0.0015 \pm 0.0004$   |
|               |                   |  |
| 112.5         | 61.4              | $0.0022 \pm 0.0004$                          |
| 117.5         | 58.0              | $0.0013 \pm 0.0004$                          |
| 122.5         | 51.0              | $0.0006 \pm 0.0004$                          |
| 127.5         | 47.5              | $0.0010 \pm 0.0004$                          |
| 132.5         | 50.0              | $0.0015 \pm 0.0005$                          |
| 137.5         | 60.0              | $0.0007 \pm 0.0005$                          |
| 142.5         | 45.0              | $0.0012 \pm 0.0006$                          |
| 147.5         | 39.0              | $0.0002 \pm 0.0004$                          |
| 152.5         | 39.3              | $0.0002 \pm 0.0004$<br>$0.0014 \pm 0.0004$   |
|               |                   |  |
| 157.5         | 48.8              | $0.0012 \pm 0.0004$                          |
| 162.5         | 51.7              | $0.0009 \pm 0.0004$                          |
| 167.5         | 55.0              | $0.0019 \pm 0.0004$                          |
| 172.5         | 62.0              | $0.0016 \pm 0.0004$                          |
| 177.5         | 65.9              | $0.0015 \pm 0.0004$                          |
| 177.5         | 65.9              | $0.0015 \pm 0.0004$                          |
| 182.5         | 69.0              | $0.0028 \pm 0.0005$                          |
| 187.5         | 77.2              | $0.0023 \pm 0.0005$                          |
| 192.5         | 94.0              | $0.0017 \pm 0.0004$                          |
| 197.5         | 97.7              | $0.0017 \pm 0.0004$<br>$0.0016 \pm 0.0005$   |
| 202.5         | 97.7              | $0.0010 \pm 0.0003$<br>$0.0020 \pm 0.0005$   |
|               |                   |  |
| 207.5         | 103.0             | $0.0015 \pm 0.0005$                          |
| 212.5         | 114.1             | $0.0014 \pm 0.0005$                          |
| 217.5         | 118.3             | $0.0009 \pm 0.0004$                          |
| 222.5         | 122.3             | $0.0019 \pm 0.0005$                          |
| 227.5         | 125.9             | $0.0020 \pm 0.0005$                          |
| 232.5         | 135.0             | $0.0013 \pm 0.0005$                          |
| 237.5         | 150.5             | $0.0014 \pm 0.0006$                          |
| 242.5         | 157.7             | $0.0011 \pm 0.0005$                          |
| 247.5         | 157.7             | $0.0001 \pm 0.0003$<br>$0.0004 \pm 0.0004$   |
|               |                   |  |
| 252.5         | 167.0             | $0.0018 \pm 0.0005$                          |
| 257.5         | 170.0             | $0.0013 \pm 0.0005$                          |
| 262.5         | 173.2             | $0.0018 \pm 0.0006$                          |
| 267.5         | 179.5             | $0.0022 \pm 0.0006$                          |
| 272.5         | 185.9             | $0.0008 \pm 0.0005$                          |
| 277.5         | 188.0             | $0.0012 \pm 0.0006$                          |
| 282.5         | 210.0             | $0.0006 \pm 0.0005$                          |
| 287.5         | 200.0             | $0.0007 \pm 0.0006$                          |
| 292.5         | 200.0             | $0.0017 \pm 0.0000$<br>$0.0004 \pm 0.0006$   |
|               |                   |  |
| 297.5         | 205.0             | $0.0009 \pm 0.0006$                          |

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- [123] Kinematically, an electron scattered through angle  $\theta_e$  transfers momentum  $\vec{q}$  and energy  $\omega$  with  $Q^2 = \vec{q}^2 \omega^2$ . The ejected proton has mass  $m_p$ , momentum  $\vec{p}_p$ , energy  $E_p$ , and kinetic energy  $T_p$ . In QE kinematics,  $\omega \approx Q^2/2m_p$ . The cross section is typically measured as a function of missing energy  $E_{\rm miss} = \omega T_p T_{\rm recoil}$  and missing momentum  $P_{\rm miss} = |\vec{q} \vec{p}_p|$ .  $T_{\rm recoil}$  is the kinetic energy of the residual nucleus. The lab polar angle between the ejected proton and virtual photon is  $\theta_{pq}$  and the azimuthal angle is  $\phi$ .  $\theta_{pq} > 0^\circ$  corresponds to  $\phi = 180^\circ$ ,  $\theta_p > \theta_q$ , and  $+P_{\rm miss}$ .  $\theta_{pq} < 0^\circ$  corresponds to  $\phi = 0^\circ$ ,  $\theta_p < \theta_q$ , and  $-P_{\rm miss}$ .
- [124] In the first Born approximation, the unpolarized (e, e'p) cross section can be expressed as the sum of four independent response functions:  $R_L$  (longitudinal),  $R_T$  (transverse),  $R_{LT}$  (longitudinal-transverse interference, and  $R_{TT}$  (transverse-transverse interference).
- [125] In the Non-relativistic Plane-Wave Impulse Approximation (NRPWIA), the transverse amplitude in the  $R_{LT}$  response is uniquely determined by the convection current. At higher  $Q^2$ , it is well-known that the convection current yields small matrix elements. As a result, the NRIA contributions which dominate  $R_L$  and  $R_T$  are suppressed in  $R_{LT}$  (and thus  $A_{LT}$ ). Hence, these observables are particularly sensitive to any mechanisms beyond the IA, such as channel coupling and relativistic and two-body current mechanisms [99].
- [126]  $A_{LT} \equiv \frac{\sigma(\phi=0^{\circ}) \sigma(\phi=180^{\circ})}{\sigma(\phi=0^{\circ}) + \sigma(\phi=180^{\circ})}$ .  $A_{LT}$  is a particularly useful quantity for experimentalists because it is systematically much less challenging to extract than either an absolute cross section or a response function.
- [127] s-shell nucleons are generally knocked out from high-density regions of the target nucleus. In these high-density regions, the IA is expected to be less valid than for knockout from the valence p-shell states lying near the surface. In this region of "less-valid" IA, sizeable contributions to the s-shell cross sections arise from two-nucleon current contributions stemming from Meson-Exchange Currents (MEC) and Intermediate  $\Delta(1232)$ -Isobar Creation (IC). In addition to affecting the single-nucleon knockout cross sections, the two-nucleon cur-

- rents can result in substantial multi-nucleon knockout contributions to the higher  $E_{\rm miss}$  continuum cross sections [99].
- [128] The transverse-longitudinal difference is  $S_T S_L$ , where  $S_X = \sigma_{\text{Mott}} V_X R_X / \sigma_X^{ep}$ , and  $X \in \{T, L\}$ .  $\sigma_X^{ep}$  represents components of the off-shell ep cross section and may be calculated using the CCX prescriptions of deForest [87, 122].
- [129] When necessary, the differential dependencies of the measured cross sections were changed to match those employed in the theoretical calculations. The pristine detection volume  $\Delta V_b(E_{\rm miss}, P_{\rm miss}, \omega, Q^2)$  was changed to a weighted detection volume by weighting each of the trials with the appropriate Jacobian(s).
- [130] The difference between cross sections averaged over the spectrometer acceptances and calculated for a small region of the central kinematics was no more than 1%. Thus, the finite acceptance of the spectrometers was not an issue.
- [131] This Jacobian is given by  $\frac{\partial E_{\text{miss}}}{\partial p_p} = \frac{p_p}{E_p} + \frac{\vec{p}_p \cdot \vec{p}_{\text{recoil}}}{p_p E_{\text{recoil}}},$  where  $E_{\text{recoil}} = \sqrt{p_{\text{recoil}}^2 + m_{\text{recoil}}^2}.$ [132] The kinematic factor  $K = \frac{p_p E_p}{8\pi^3}$ , while  $\sigma_{\text{Mott}} = \frac{2}{3} e^{-\frac{2}{3}} e^{-\frac{2}{3}} e^{-\frac{2}{3}} e^{-\frac{2}{3}} e^{-\frac{2}{3}}$
- [132] The kinematic factor  $K = \frac{p_p E_p}{8\pi^3}$ , while  $\sigma_{\text{Mott}} = \frac{\alpha^2 \cos^2(\theta_e/2)}{4E_0^2 \sin^4(\theta_e/2)}$ . The dimensionless kinematic factors are as follows:  $v_L = \frac{Q^4}{\bar{q}^4}$ ,  $v_T = \frac{Q^2}{2\bar{q}^2} + \tan^2(\theta_e/2)$ ,  $v_{LT} = \frac{Q^2}{\bar{q}^2} \sqrt{\frac{Q^2}{\bar{q}^2} + \tan^2(\theta_e/2)}$ , and  $v_{TT} = \frac{Q^2}{2\bar{q}^2}$ . The five-fold differential cross sections  $\frac{d^5\sigma}{d\omega_e d\Omega_p}$  for proton removal from the 1p-shell result from integrating over the appropriate bound-state region of  $E_{\text{miss}}$  and decompose in a similiar manner save for an additional multiplicative recoil factor given by  $f_{\text{recoil}} = \left[1 \frac{E_p}{E_{\text{recoil}}} \frac{\vec{F}_{\text{miss}} \cdot \vec{r}_p}{p_p^2}\right]$ .
- [133] The accuracy of the response function separation depends on precisely matching the values of  $|\vec{q}|$  and  $\omega$  at each of the different kinematic settings. This precise matching was achieved by measuring  $^1{\rm H}(e,ep)$  with a pinhole collimator placed in front of the HRS<sub>e</sub>. The proton momentum was thus  $\vec{q}$ . The  $^1{\rm H}(e,ep)$  proton momentum peak was determined to  $\delta p/p = 1.5 \times 10^{-4}$ , which allowed for an identical matching of  $\delta |\vec{q}|/|\vec{q}|$  between the different kinematic settings.
- $[134] R_{L+TT} \equiv R_L + \frac{V_{TT}}{V_L} R_{TT}$
- [135] The nucleon current was calculated using a fully relativistic operator, and the wave functions were four-component spinor solutions of the Dirac equation including scalar and vector potentials.
- [136] Strictly speaking, the longitudinal response function  $R_L$  could not be separated from the perpendicular kinematics data. However, since both Kelly and Udías et al. calculate the term  $\frac{v_{TT}}{v_L}R_{TT}$  to be < 10% of  $R_{L+TT}$  in these kinematics,  $R_L$  and  $R_{L+TT}$  responses are both presented on the same plot.
- [137] The quantity y (which is the minimum value of the initial momentum of the nucleon) is generally used to label non-QE kinematics. According to Kelly [2],  $y = -\frac{|\vec{q}|}{2} + \frac{m_N \omega}{|\vec{q}|} \sqrt{\frac{\vec{q} \cdot \vec{q}}{Q^2} (1 + \frac{Q^2}{4m_N^2})}, \text{ which for these kinematics, is } 0.22. \ y = 0 \text{ for QE kinematics.}$